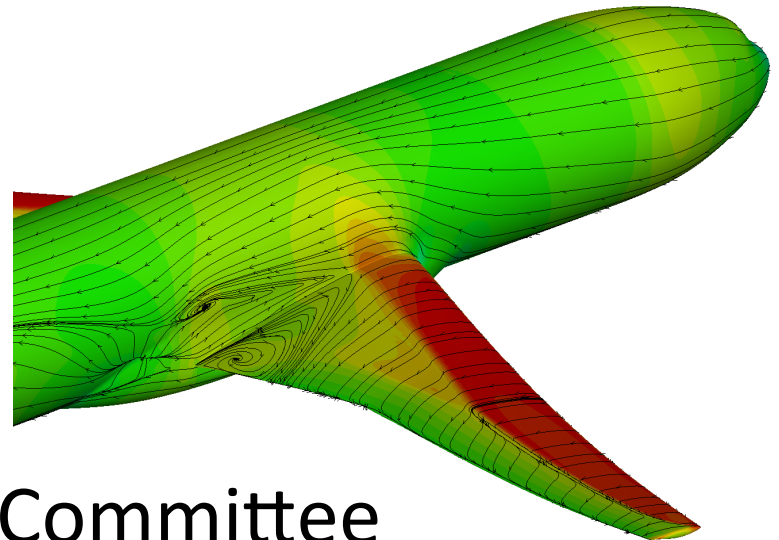


DPW 5 Summary of Participant Data

Ed Tinoco,
David Levy,
Olaf Brodersen,
and the DPW Organizing Committee



24 June 2012



5th CFD Drag Prediction Workshop

New Orleans, Louisiana – June 2012

Outline:

- Participant Data
- Case 1: Grid Convergence
- Case 2: Buffet Study
- Pressure Data
- Side of Body Separation
- Trailing Edge Separation
- Conclusions



Participant Data:

- **54 Data Total Data Submittals**
- **22 Teams/Organizations**
 - 10 N. America, 5 Europe, 6 Asia, 1 S. America
 - 8 Government, 5 Industry, 6 Academia, 2 Commercial, 1 Unknown
 - 1 for Case 3 only
- **Grid Types:**
 - 5 Overset (4 Teams)
 - 7 Structured Multi-block (5 Teams)
 - 25 Unstructured (13 teams)
 (14 Hex, 7 Hybrid, 4 Prism)
 - 16 Custom (all types)
- **Turbulence Models:**
 - 34 SA (all types), 12 SST, 4 k-e-RT, 1 EARSM, 1 Lag-RST



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Team	ID	Name	Organization	File Name	Code	Misc Solver	Grid Type	Turbulence Model
1	A	Sclafani	Boeing (Huntington)	SclafaniT-CommonOverset-SA1a-1	OVERFLOW v2.2c	Central	Overset	SA-1a
	B	Sclafani	Boeing (Huntington)	SclafaniT-CommonOverset-SARC-1	OVERFLOW v2.2c	Central	Overset	SA-1a w/ RC
	C	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SA1a-1	OVERFLOW v2.2c	Central	Custom (Overset)	SA-1a
	D	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SA1a-2	OVERFLOW v2.2c	Central / QCR	Custom (Overset)	SA-1a
	E	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-1	OVERFLOW v2.2c	Central	Custom (Overset)	SA-1a w/ RC
	F	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-2	OVERFLOW v2.2c	Central / QCR	Custom (Overset)	SA-1a w/ RC
	G	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-3	OVERFLOW v2.2c	Central	Custom (Overset)	SA-1a w/ RC
	H	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-4	OVERFLOW v2.2c	Central / QCR	Custom (Overset)	SA-1a w/ RC
2	I	Chen	Mianyang City, China	Chen-CommonHex-SA-1	MFlow	Upwind	Hex	SA
	J	Chen	Mianyang City, China	Chen-CommonHex-SA-1	MFlow	Upwind	Hybrid	SA
3	K	GariÉpy	EcolePolytechMontreal	GariÉpyM-CommonPrism-SA-1	Fluent V13	Upwind	Prism	SA
	L	GariÉpy	EcolePolytechMontreal	GariÉpyM-Custom-SA-1	Fluent V13	Upwind	Custom (Hex)	SA
4	M	Scalabrin	Embraer	ScalabrinL-CommonHex-RT-1	CFD++	Upwind	Hex	k-e-RT
	N	Scalabrin	Embraer	ScalabrinL-CommonHex-SST-1	CFD++	Upwind	Hex	SST
	O	Scalabrin	Embraer	ScalabrinL-CommonHybrid-RT-1	CFD++	Upwind	Hybrid	k-e-RT
	P	Scalabrin	Embraer	ScalabrinL-CommonHybrid-SST-1	CFD++	Upwind	Hybrid	SST
	Q	Scalabrin	Embraer	ScalabrinL-CommonPrism-RT-1	CFD++	Upwind	Prism	k-e-RT
	R	Scalabrin	Embraer	ScalabrinL-CommonPrism-SST-1	CFD++	Upwind	Prism	SST
	S	Scalabrin	Embraer	ScalabrinL-CommonCustom-RT-1	CFD++	Upwind	Custom (Hybrid)	k-e-RT
	T	Scalabrin	Embraer	ScalabrinL-CommonCustom-SST-1	CFD++	Upwind	Custom (Hybrid)	SST
5	U	Eliasson	FOI	EliassonP-CommonHex-EARSM-1	EDGE		Hex	EARSM
	V	Eliasson	FOI	EliassonP-CommonHex-SA-1	EDGE		Hex	SA
	W	Eliasson	FOI	EliassonP-CommonHex-SST-1	EDGE		Hex	SST
6	X	Powell	Gulfstream	PowellN-CommonHybrid-SA-1	FUN3D		Hybrid	SA
7	Y	Balakrishnan	Indian Inst. Science	BalakrishnanN-CommonHex-SA-1	HIFUN	Upwind	Hex	SA
8	Z	Hashimoto	JAXA	Hashimoto-CommonHex-SA-1	FaSTAR	Upwind	Hex	SA-noft2-R
	2	Hashimoto	JAXA	Hashimoto-Custom-SA-1	FaSTAR	Upwind	Custom (Hex)	SA-noft2-R



5th CFD Drag Prediction Workshop

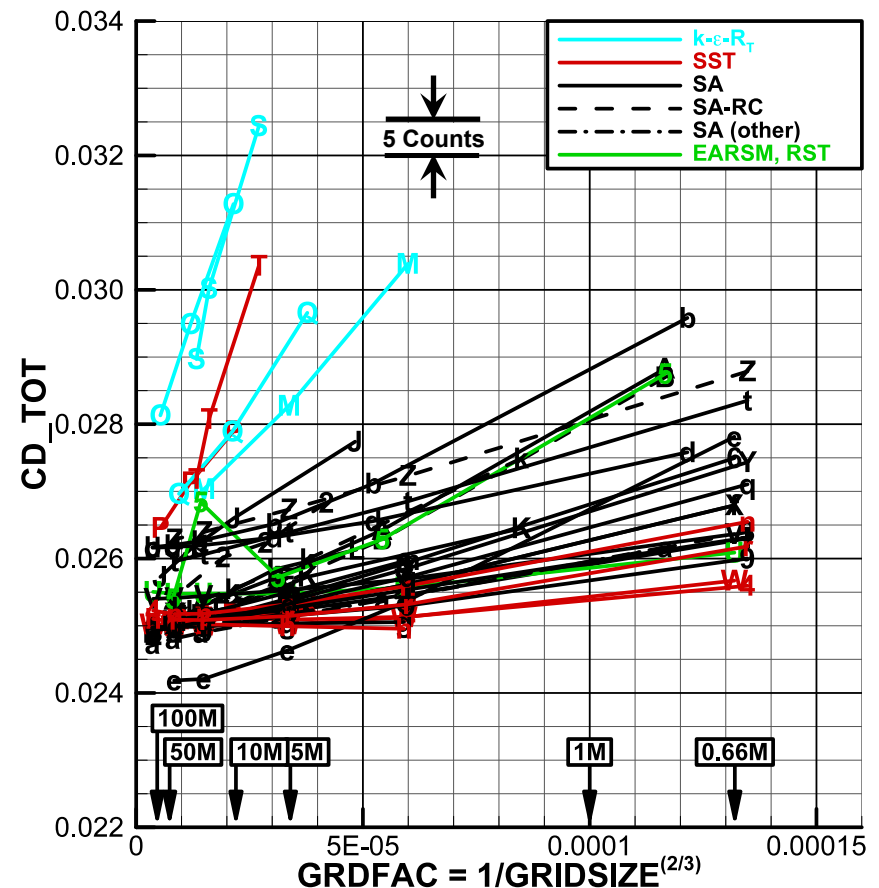
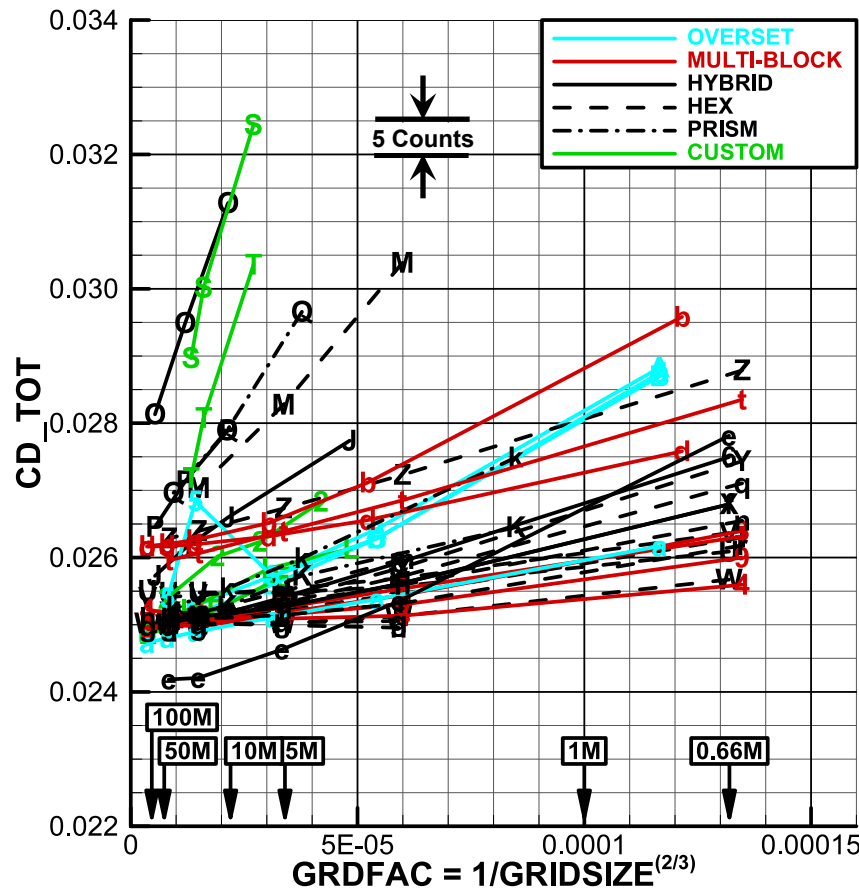
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Team	ID	Name	Organization	File Name	Code	Misc Solver	Grid Type	Turbulence Model
9	3	Yamamoto	JAXA	YamamotoK-CommonMB-SA-noft2-R-1	UPACS	Upwind	Multi-block	SA-noft2-R ($\overline{C_{rot}}=1$)
	4	Yamamoto	JAXA	YamamotoK-CommonMB-SST-V-1	UPACS	Upwind	Multi-block	SST-V
10	5	Olson	NASA Ames	Olsen-CommonOverset-LagRST-1	overflow2.2e_LRS	Central/matrix	Overset	Lag RST
11	6	Park	NASA Langley	ParkM-CommonHybrid-SA-1	FUN3D v12.2	Upwind Roe	Hybrid	SA
	7	Park	NASA Langley	ParkM-CommonMB-SA-1	CFL3D v6.6	Upwind Roe	Multi-block	SA
12	8	Cai	NPU China	CaiJ-CommonOverset-SST-1	ExStream	Upwind	Overset	SST
13	9	Hue	ONERA	HueD_CommonMB_SA_1	elsA	Central	Multi-block	SA
14	a	Coder	Penn St. U	CoderJ-CommonOverset-SA-fv3-1	OVERFLOW 2.2c	Upwind	Overset	SA-fv3
15	b	Osusky	U. Toronto	OsuskyM-CommonMB-SA-1	Diablo	Scalar	Multi-block	SA
	d	Osusky	U. Toronto	OsuskyM-CommonMB-SA-2	Diablo	Matrix	Multi-block	SA
16	e	Levy	Cessna Aircraft Co.	LevyD-CommonHybrid-SA-1	NSU3D	Central/matrix	Hybrid	SA
	f	Levy	Cessna Aircraft Co.	LevyD-CommonHybrid-SA-2	FUN3D	Upwind Roe	Hybrid	SA
17	g	Crippa	DLR	DLR_CrippaS-CommonHex-SA-1	TAU	Matrix	Hex	SA
	h	Crippa	DLR	DLR_CrippaS-CommonHex-SST-1	TAU	Matrix	Hex	SST
18	k	Moitra	CRL_INDIA	CRL_INDIA_MoitraA	CFD++	Upwind	Prism	SA-RC
19	m	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SA-1	BCFD	Upwind HLLE	Hex	SA
	n	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SSTV-1	BCFD	Upwind HLLE	Hex	SST-V
	q	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SA-2	BCFD	Upwind HLLE	Hex	SA
	r	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SSTV-2	BCFD	Upwind HLLE	Hex	SST-V
20	t	Temmerman	NUMECA	DPW-V-NUMECA	FINE/Open	Cell Centered	Multi-block	SA
21	α	Brodersen	DLR	DLR_BrodersenO_Cust1_SA_D1	TAU	Diss 1	Custom (Hybrid)	SA
	β	Brodersen	DLR	DLR_BrodersenO_Cust1_SA_D3	TAU	Diss 3	Custom (Hybrid)	SA
	δ	Brodersen	DLR	DLR_BrodersenO_Cust2_SA_D1	TAU	Diss 1	Custom (Hyb w/ Hex-Wake)	SA
	γ	Brodersen	DLR	DLR_BrodersenO_Cust2_SA_D3	TAU	Diss 3	Custom (Hyb w/ Hex-Wake)	SA
	λ	Brodersen	DLR	DLR_BrodersenO_Cust2_SST_D1	TAU	Diss 1	Custom (Hyb w/ Hex-Wake)	Menter SST
	π	Brodersen	DLR	DLR_BrodersenO_Cust2_SST_D3	TAU	Diss 3	Custom (Hyb w/ Hex-Wake)	Menter SST

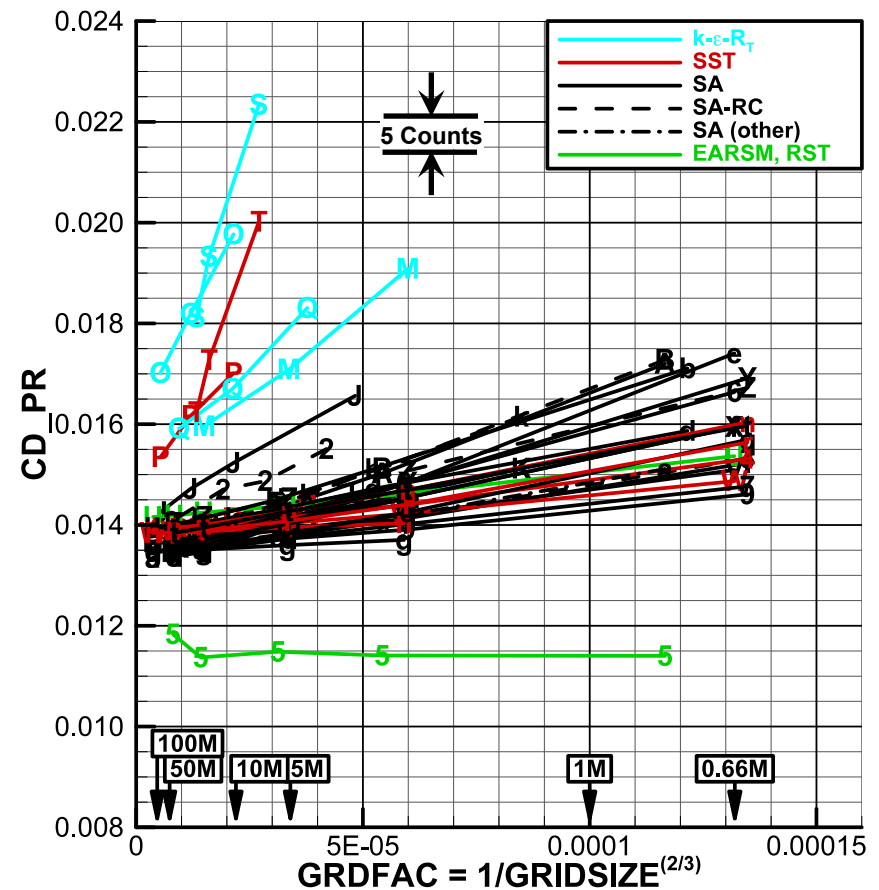
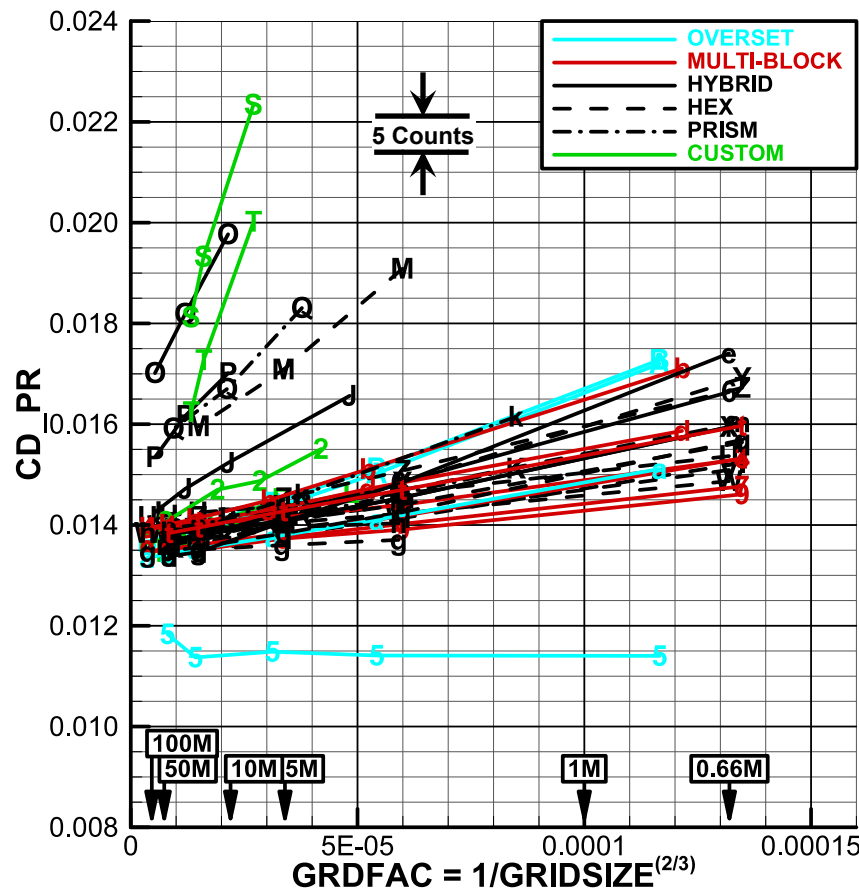
Case 1: Grid Convergence Study

- NASA Common Research Model, Wing-Body
- Mach=0.85, $C_L=0.500\pm0.001$
- Grid Resolution Level:
 - 1) Tiny 2) Coarse 3) Medium,
 - 4) Fine 5) Extra-Fine 6) Super-Fine
- Chord Reynolds Number: 5×10^6

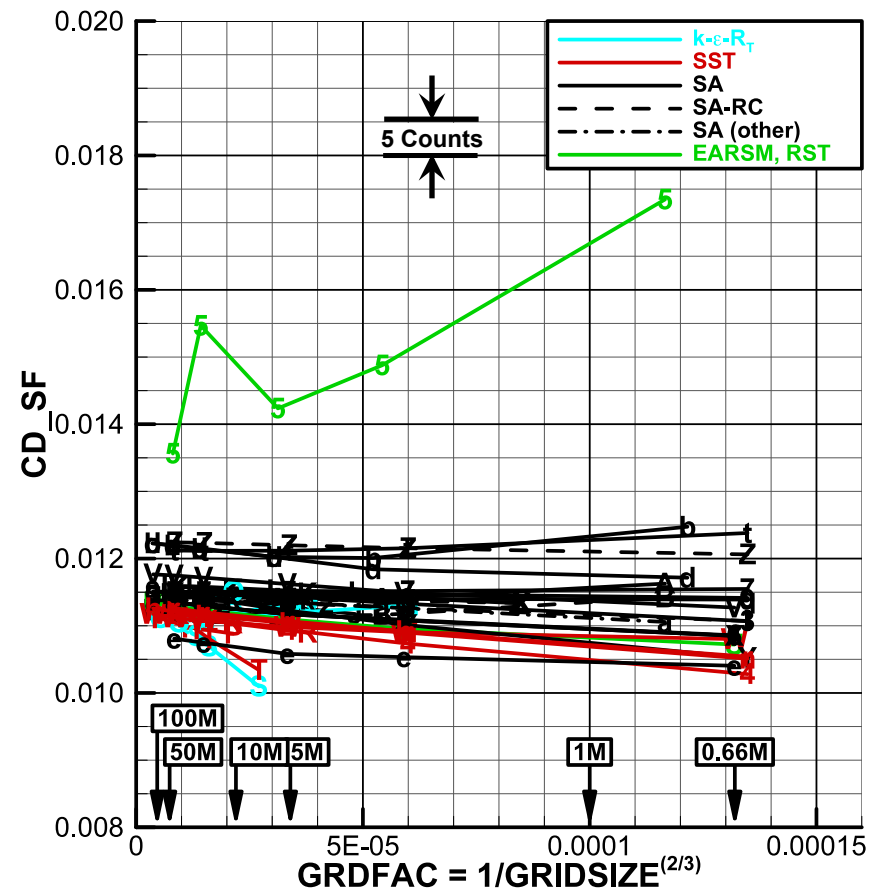
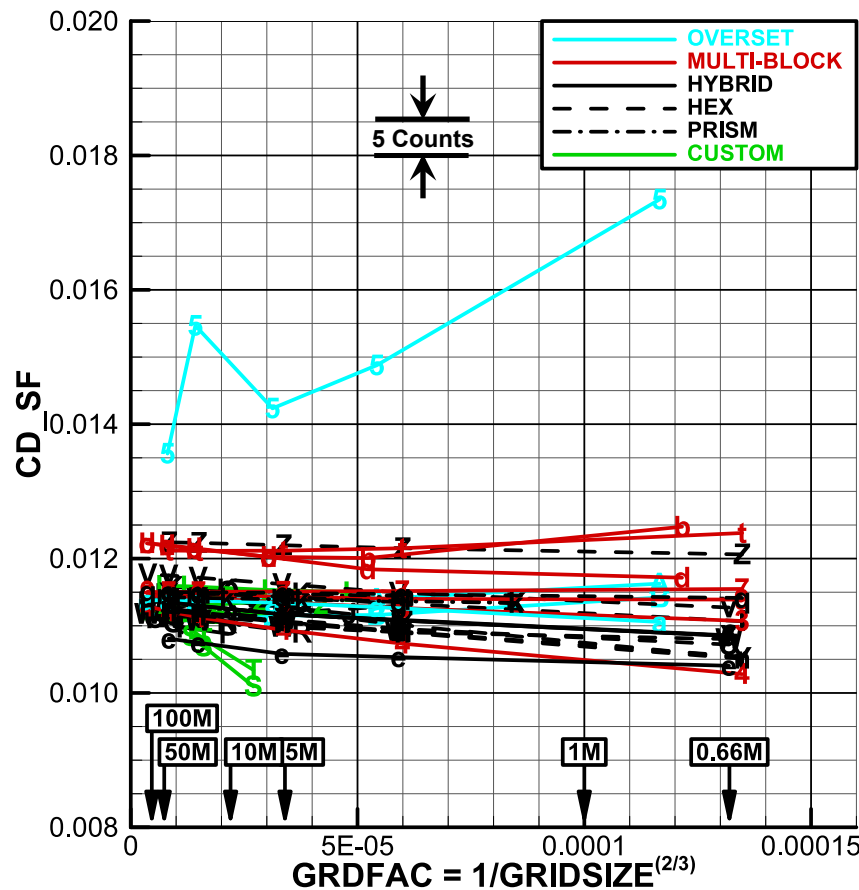
Case 1: CD_{TOT} - All Solutions by Grid Type and Turbulence Model



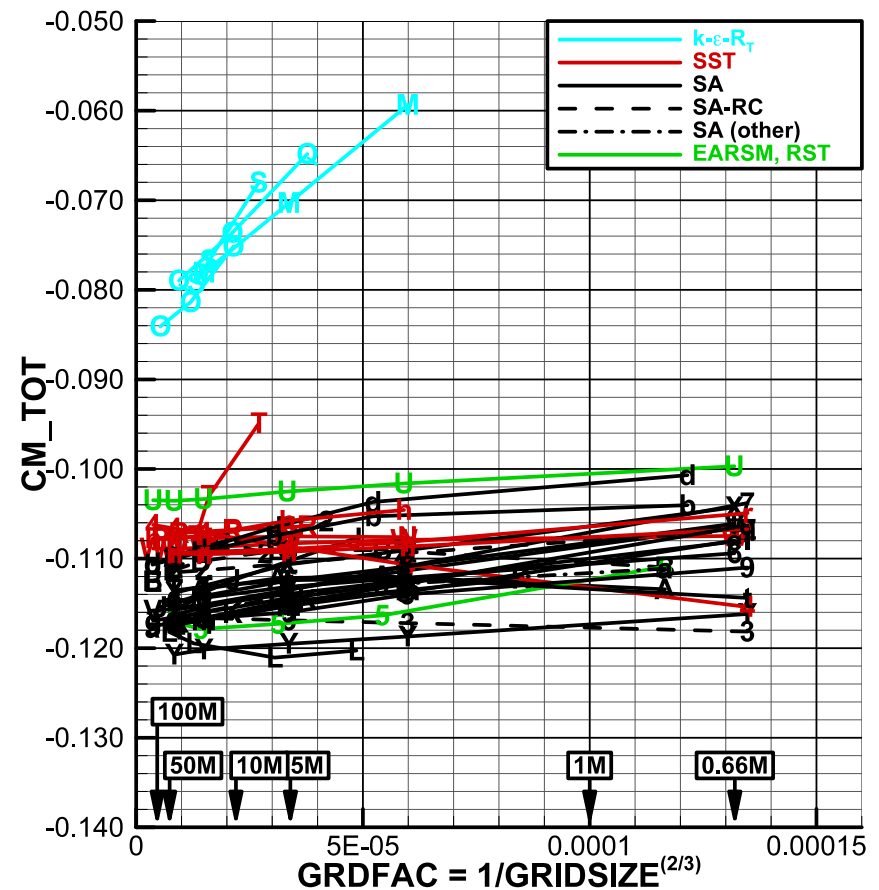
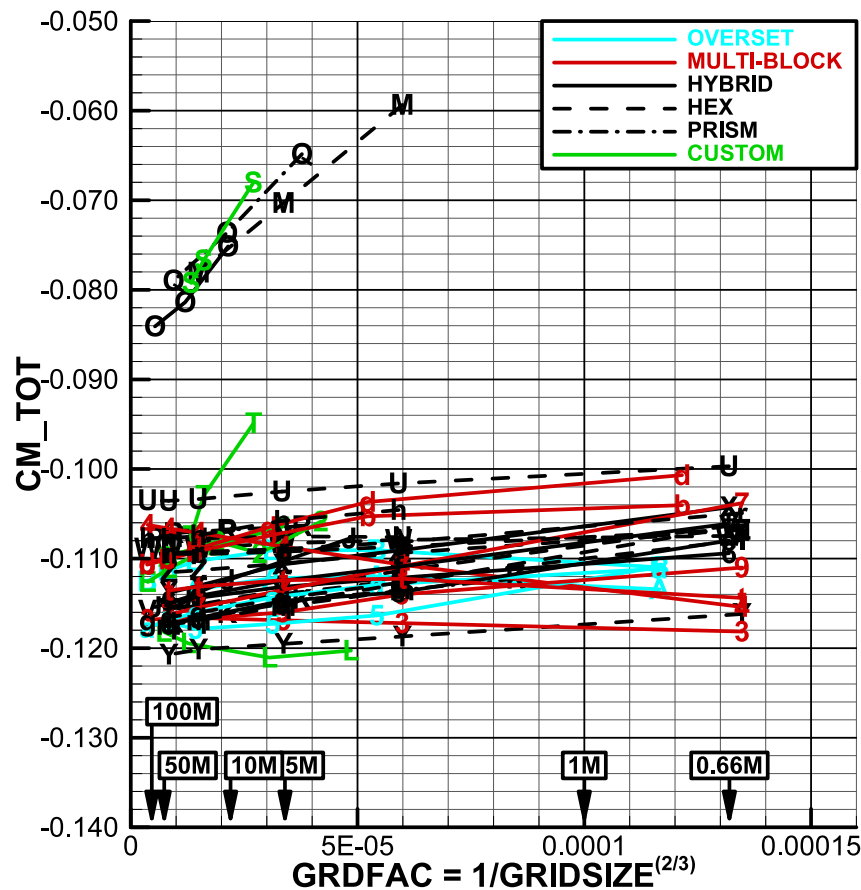
Case 1: CD_PR - All Solutions by Grid Type and Turbulence Model



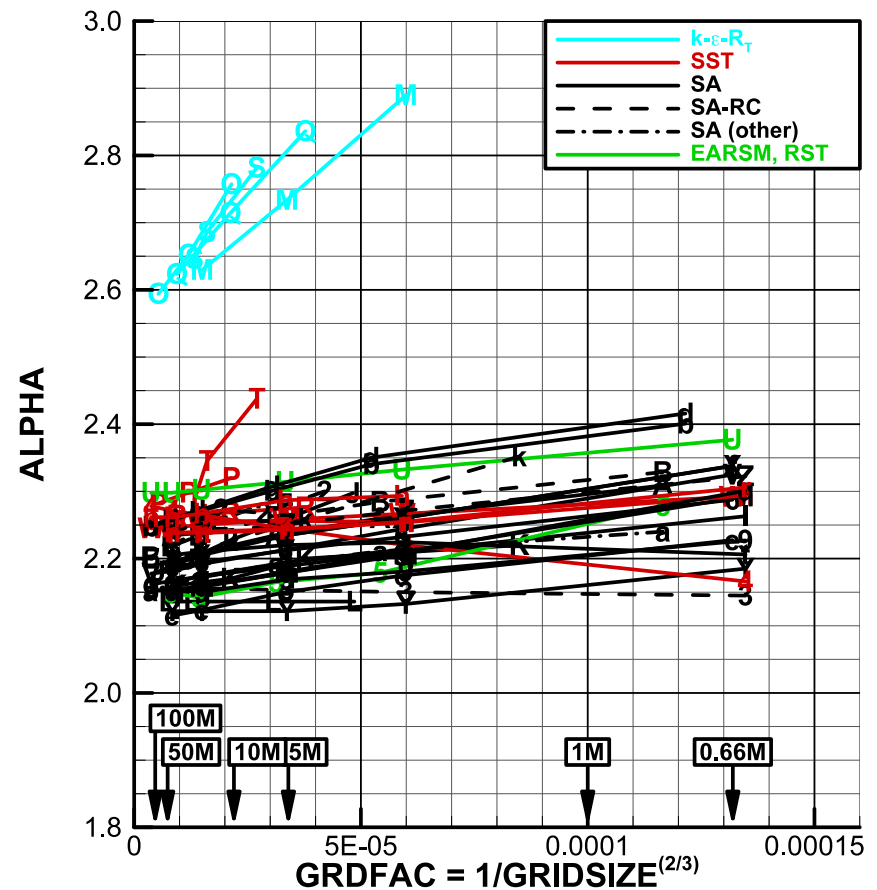
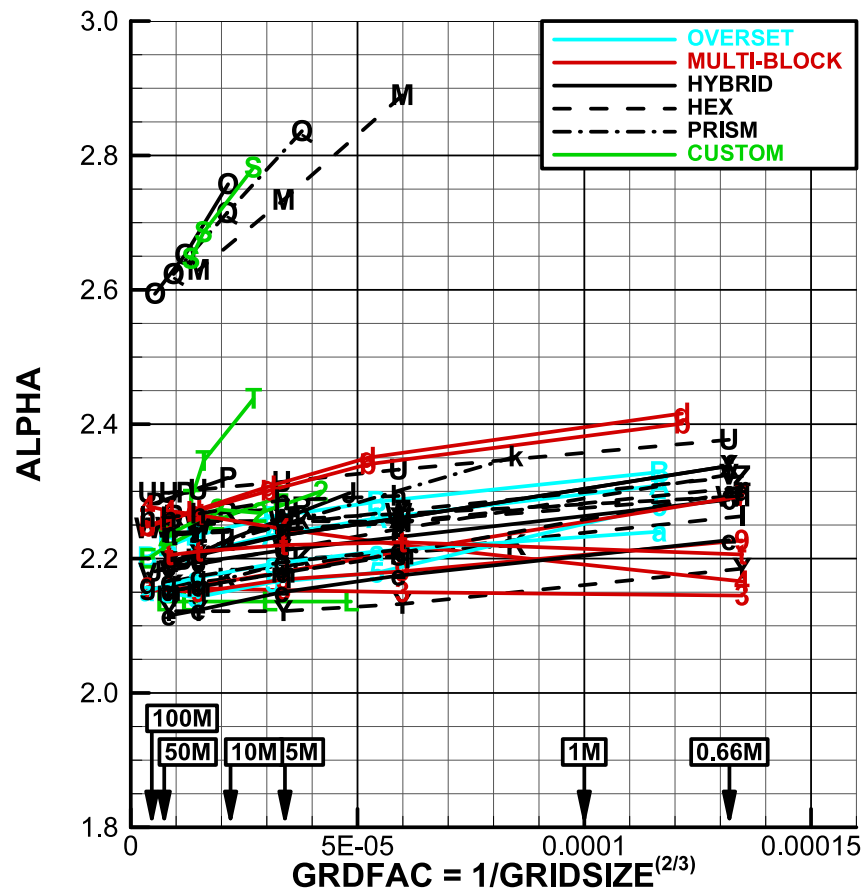
Case 1: CD_{SF} - All Solutions by Grid Type and Turbulence Model



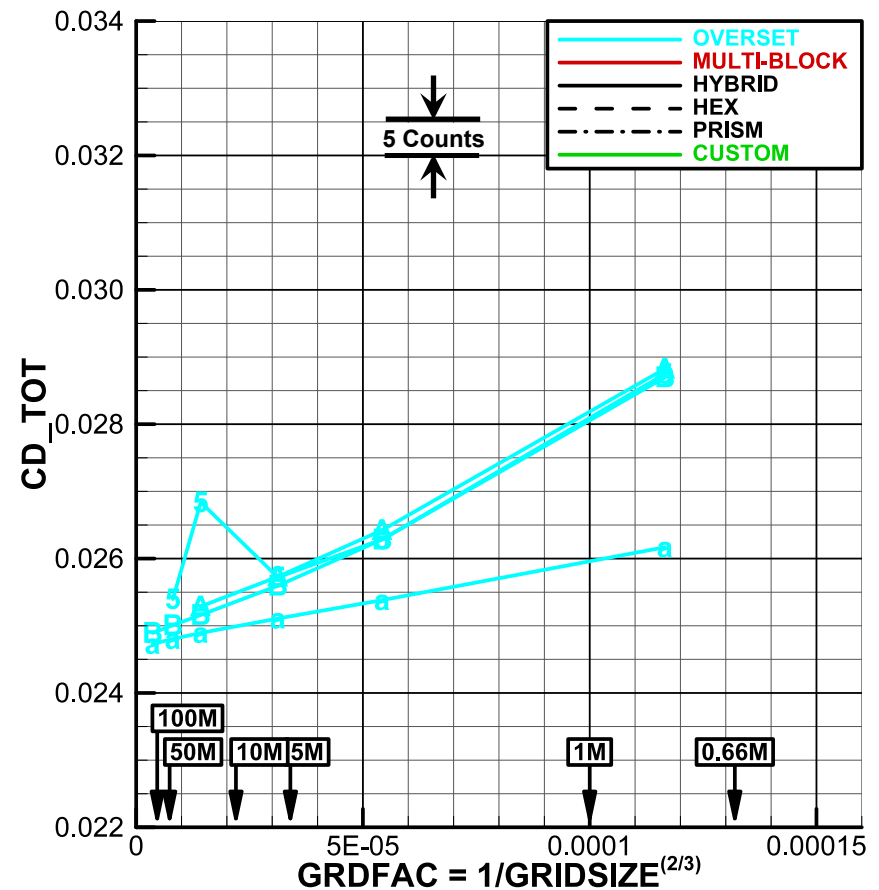
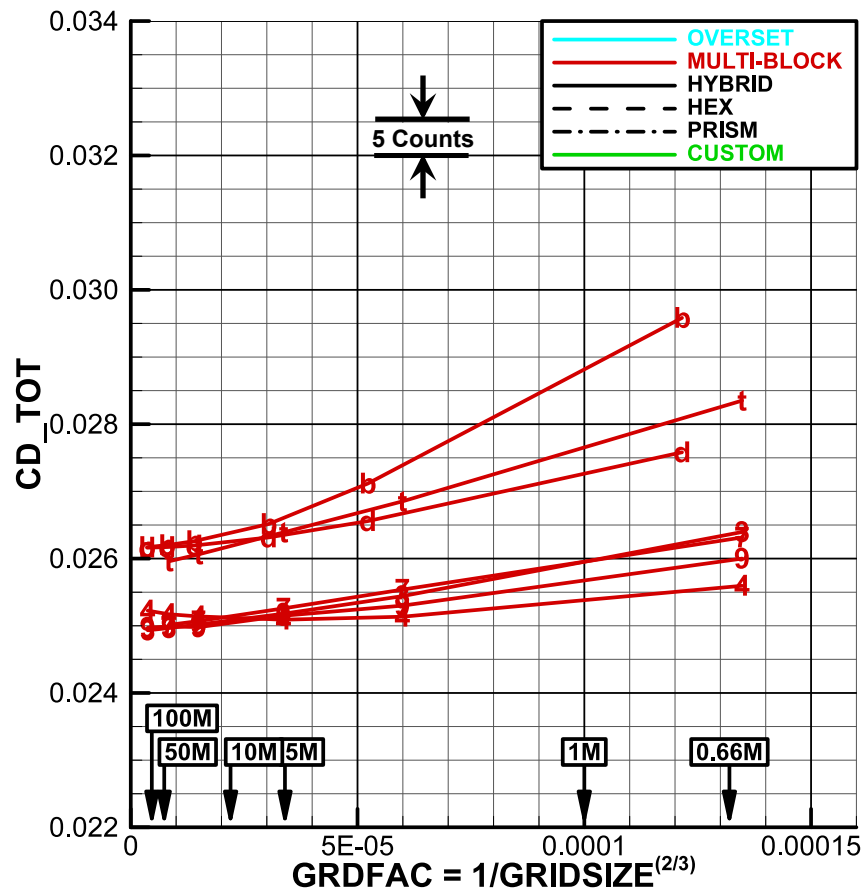
Case 1: CM_TOT - All Solutions by Grid Type and Turbulence Model



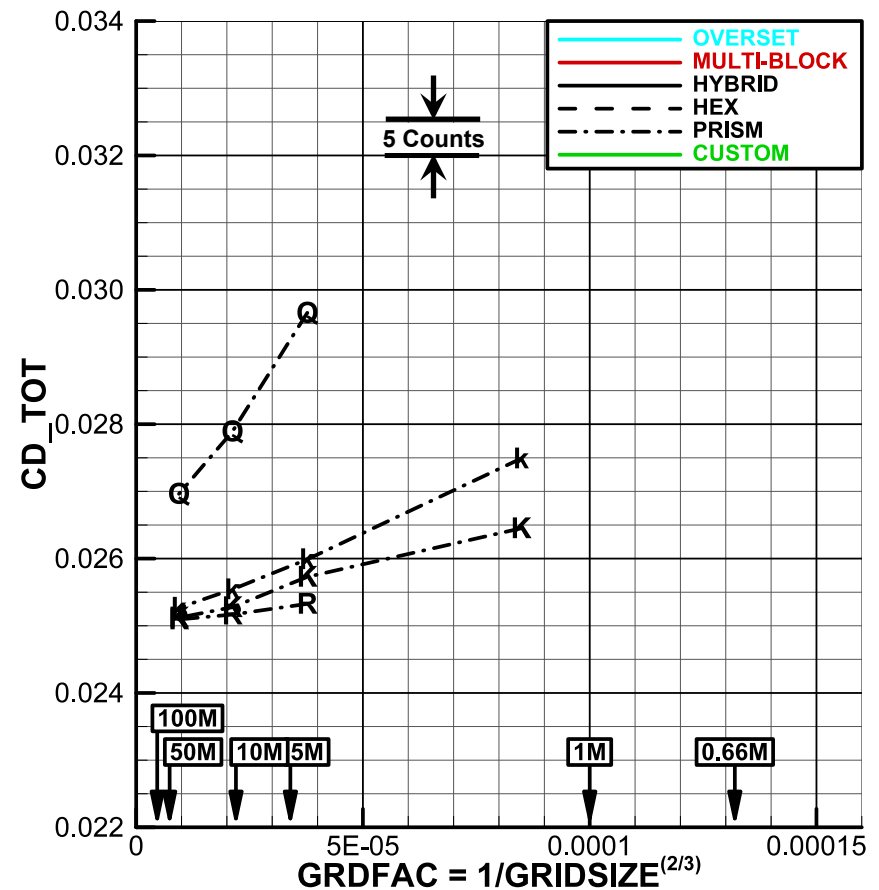
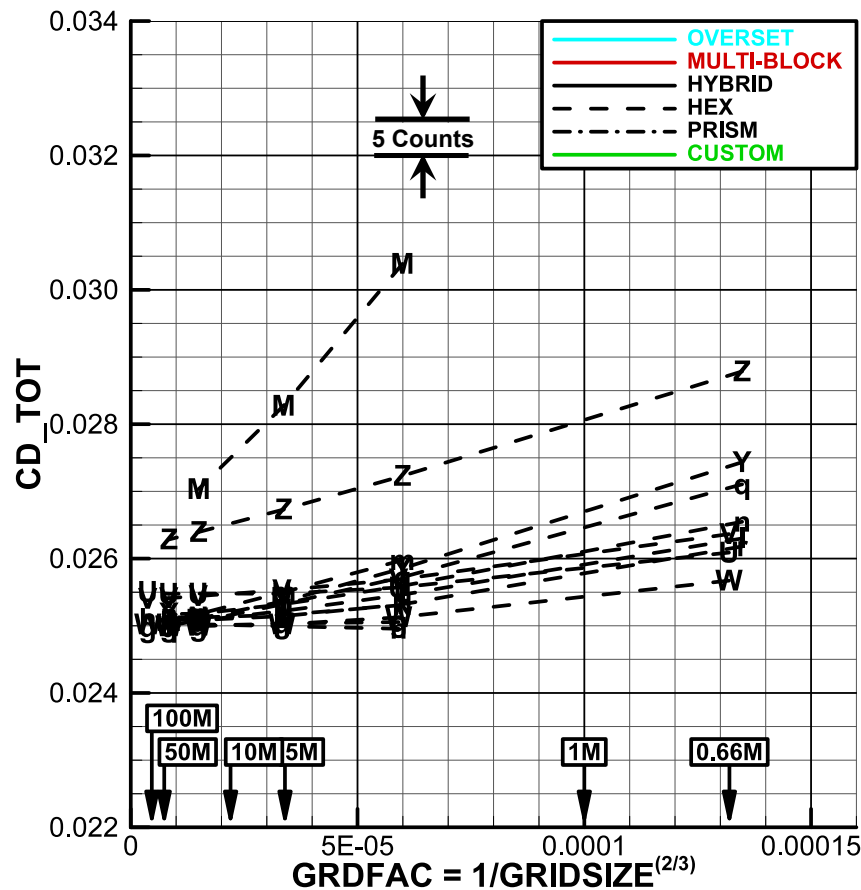
Case 1: ALPHA - All Solutions by Grid Type



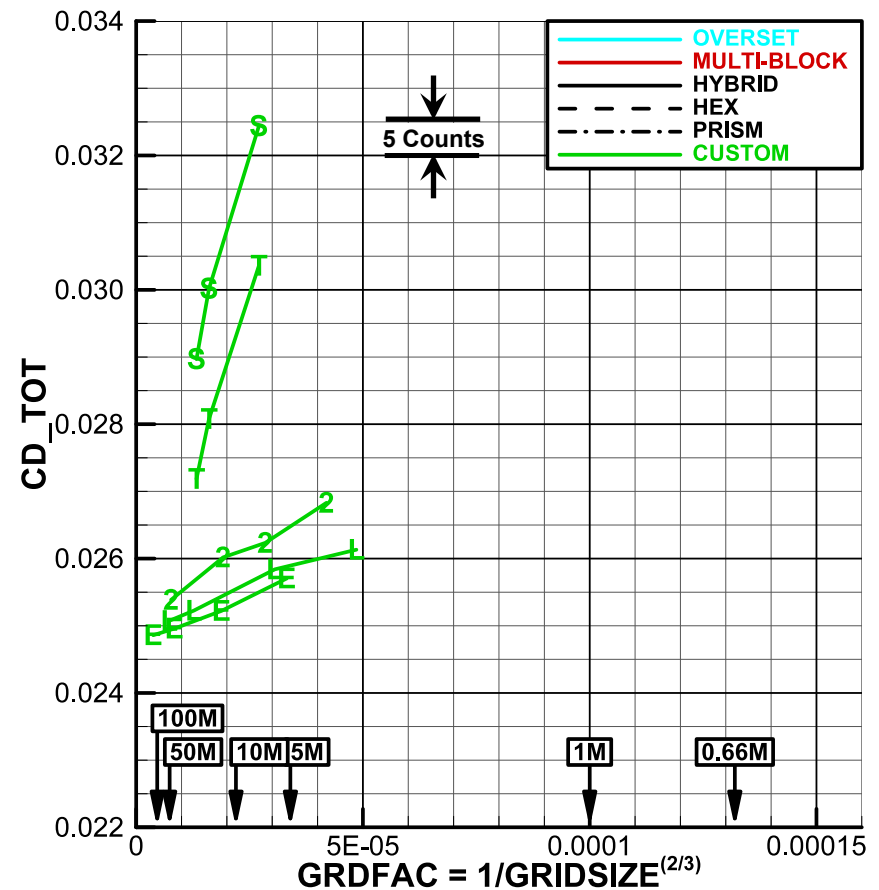
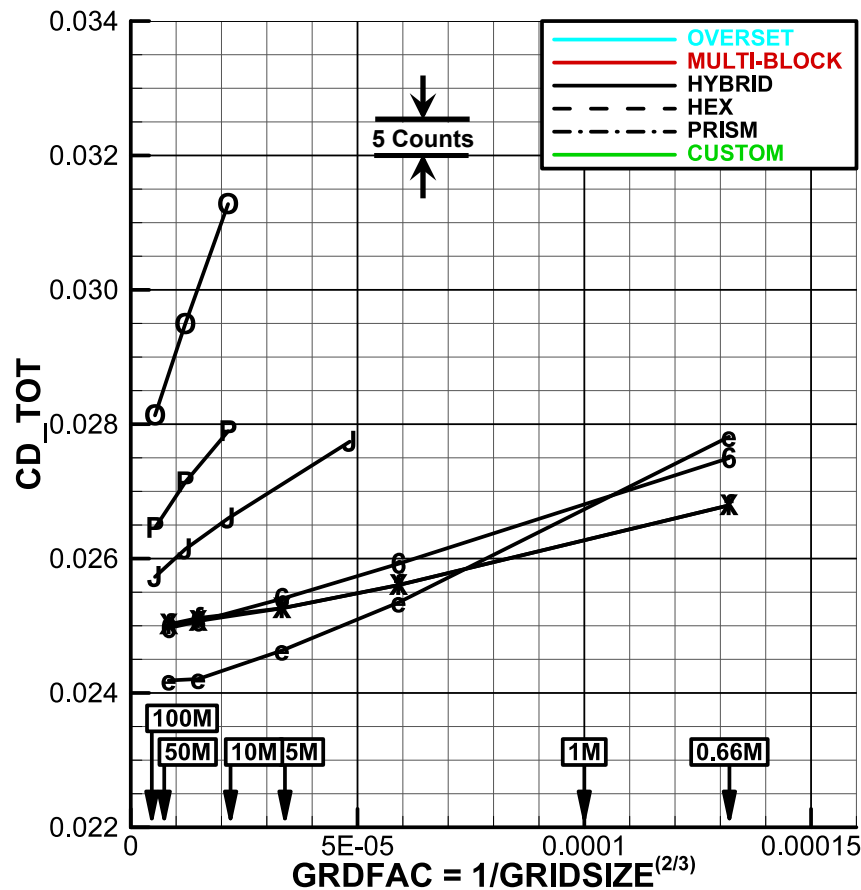
Case 1: CD_TOT – Multi-block and Overset Grids



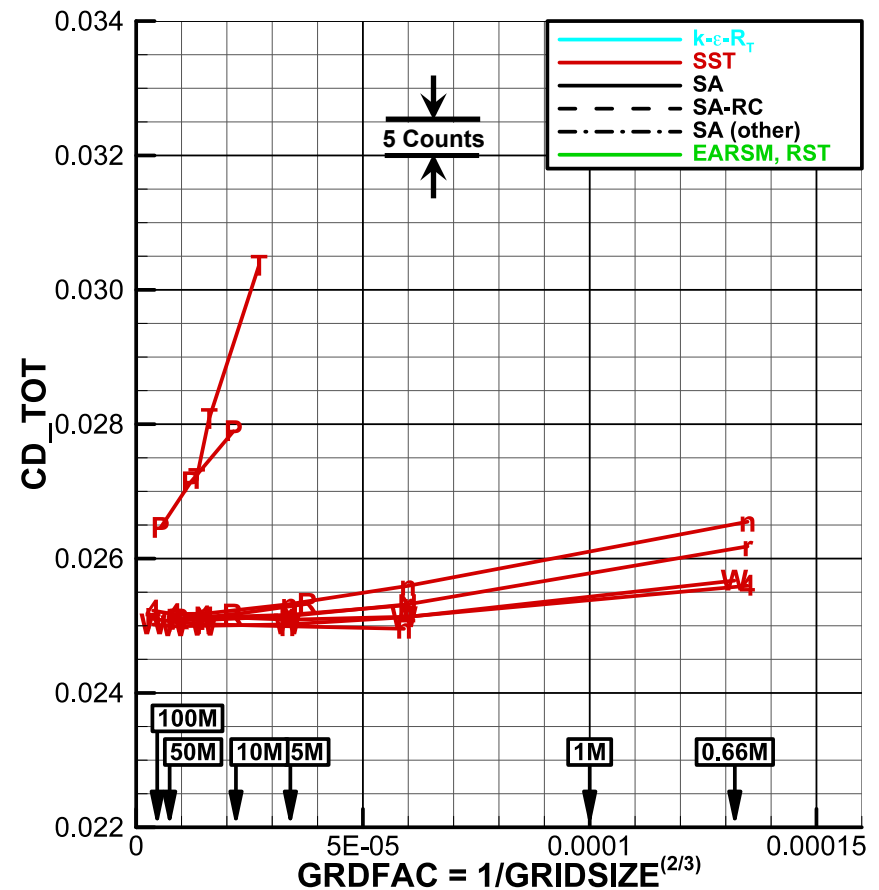
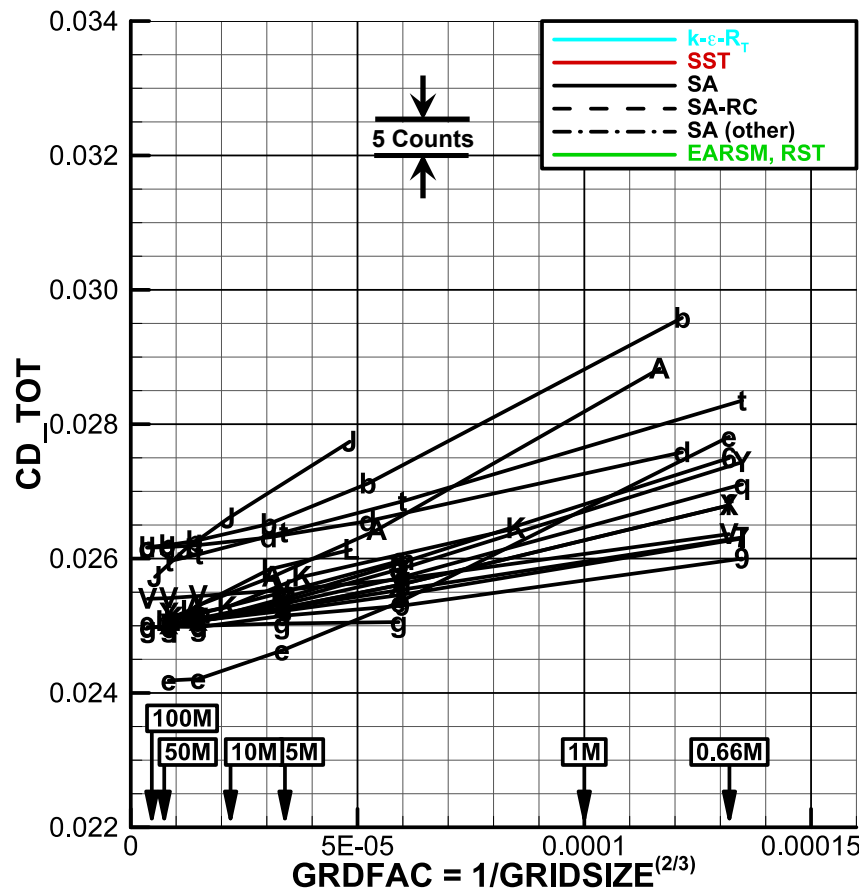
Case 1: CD_TOT – Unstructured Hexahedral and Prismatic Grids



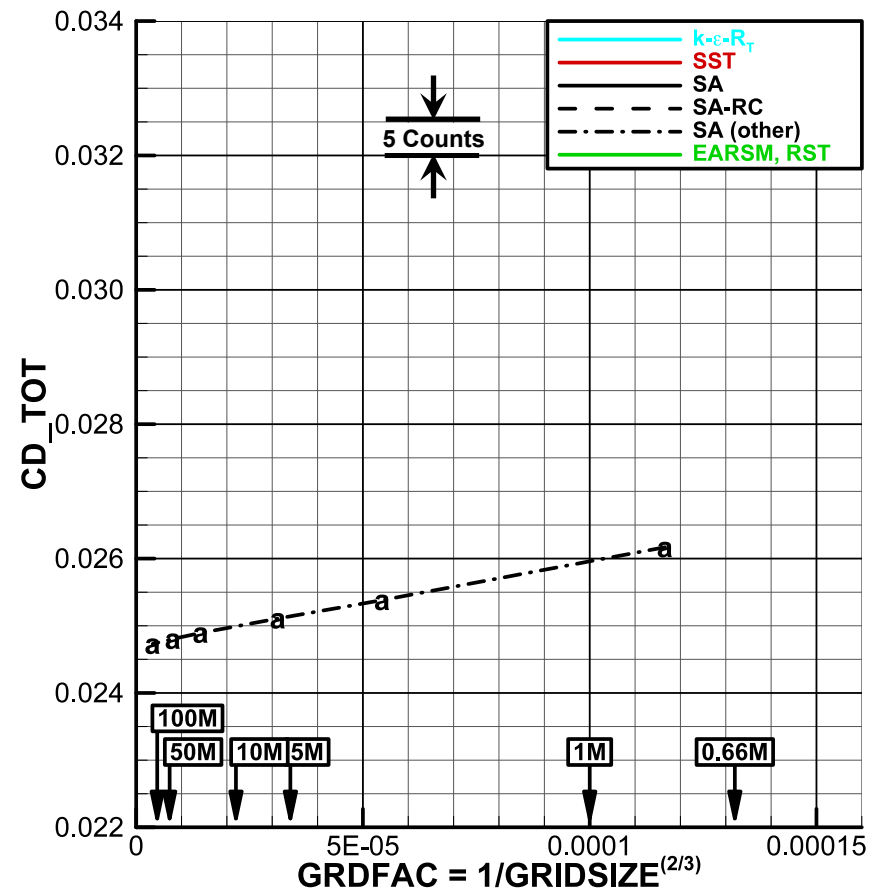
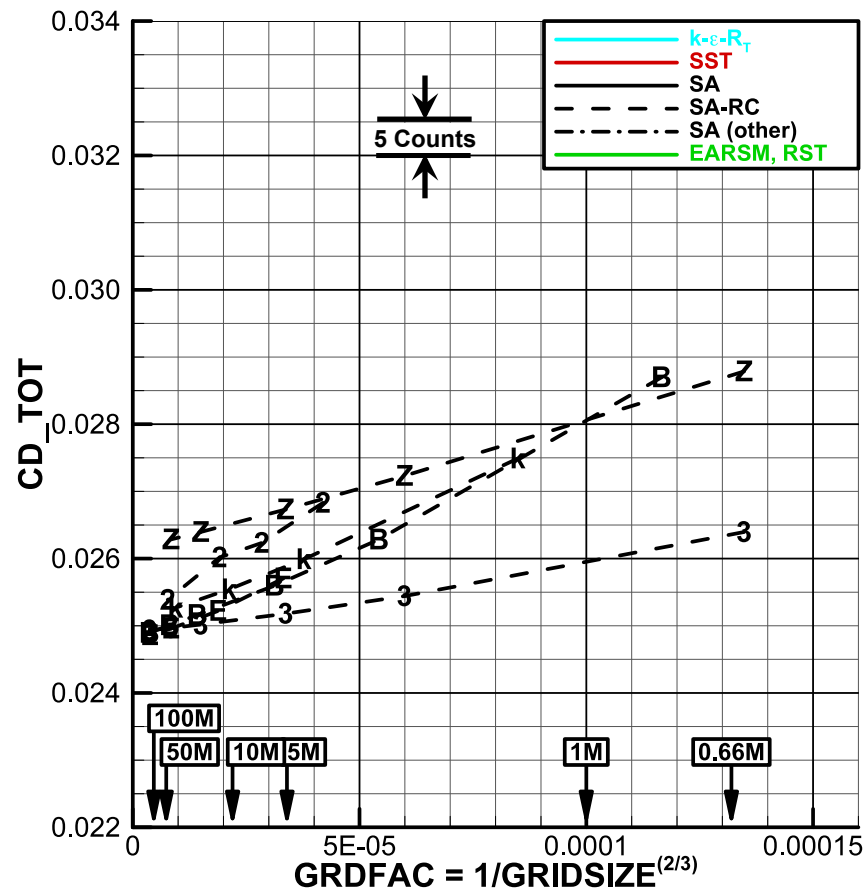
Case 1: CD_TOT – Unstructured Hybrid and all Custom Grids



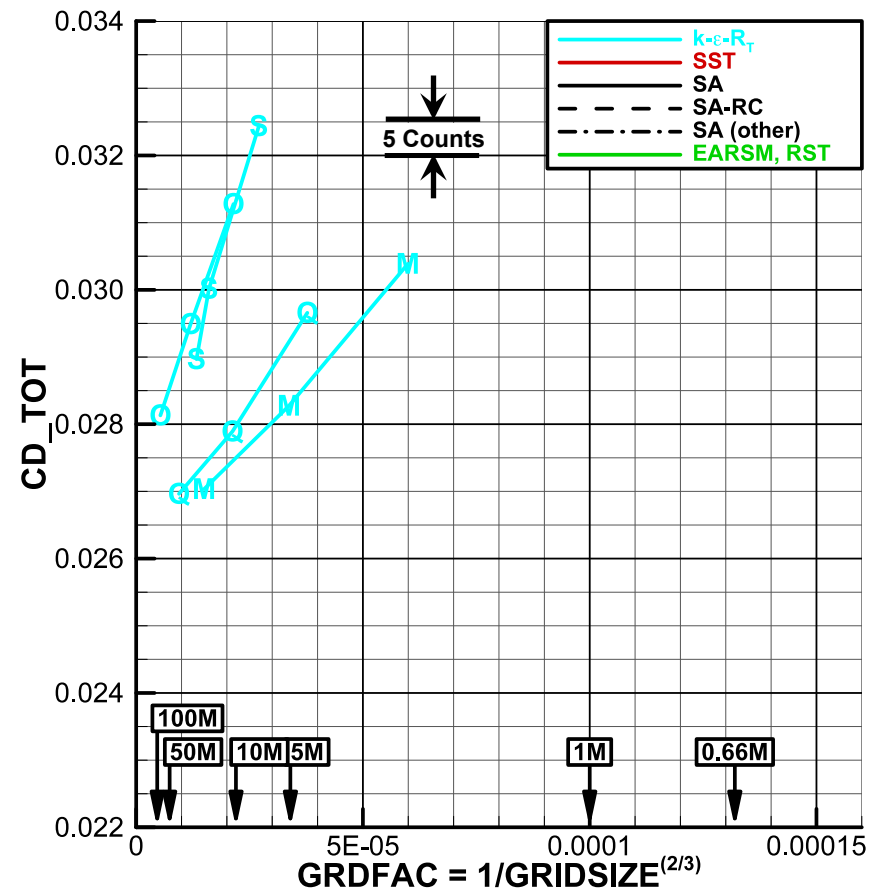
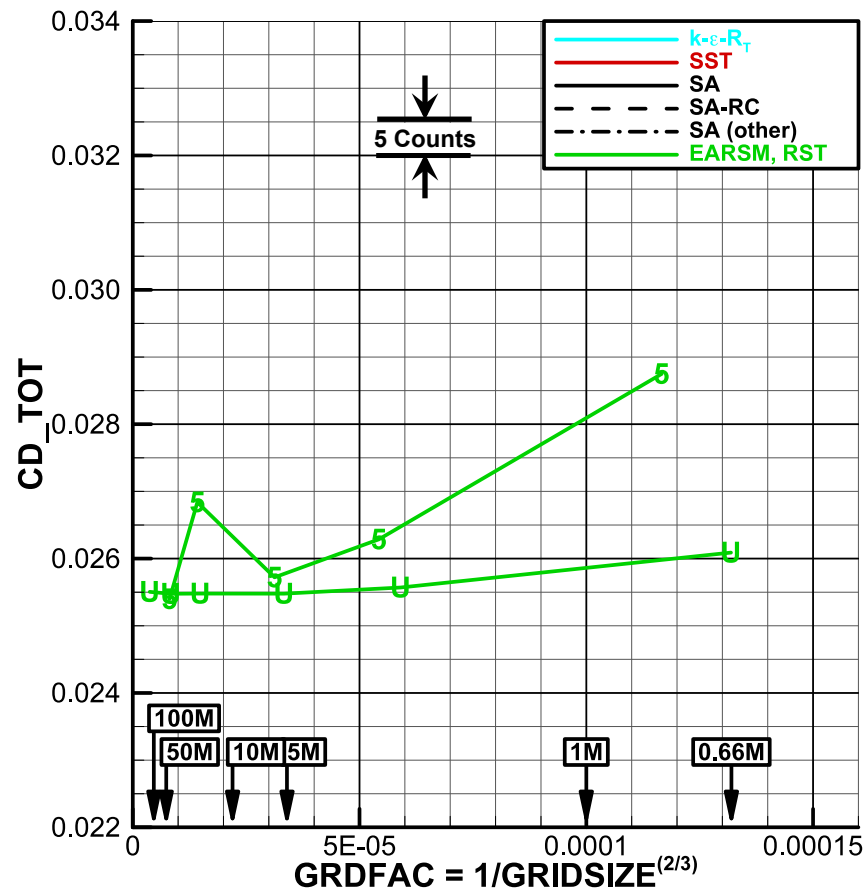
Case 1: CD_TOT – Spalart Allmaras and Shear Stress Transport Turb. Models



Case 1: CD_TOT – SA w/ Rotation Correction and SA other Turb. Models



Case 1: CD_TOT – k-ε-RT and EARSM,RST Turbulence Models

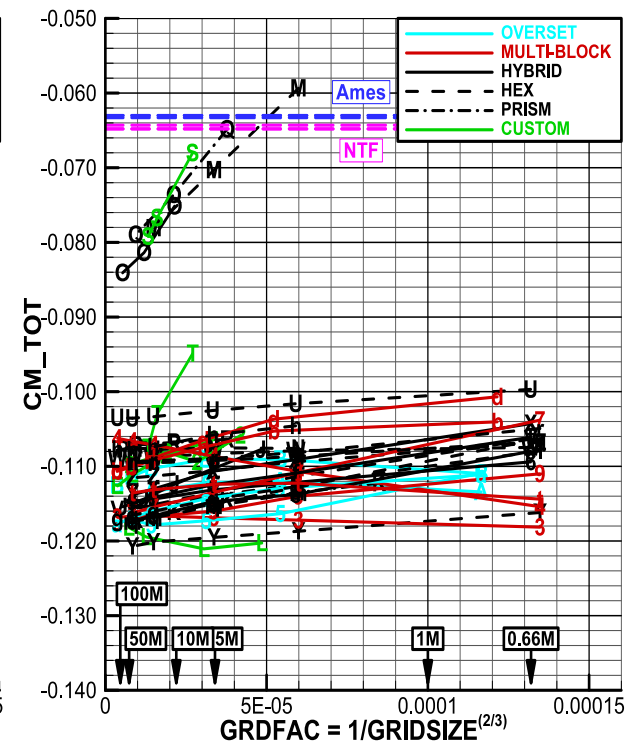
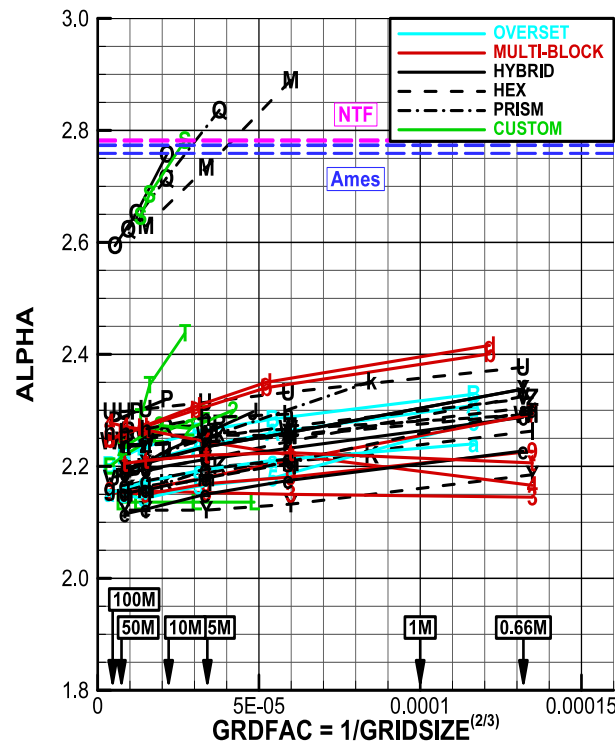
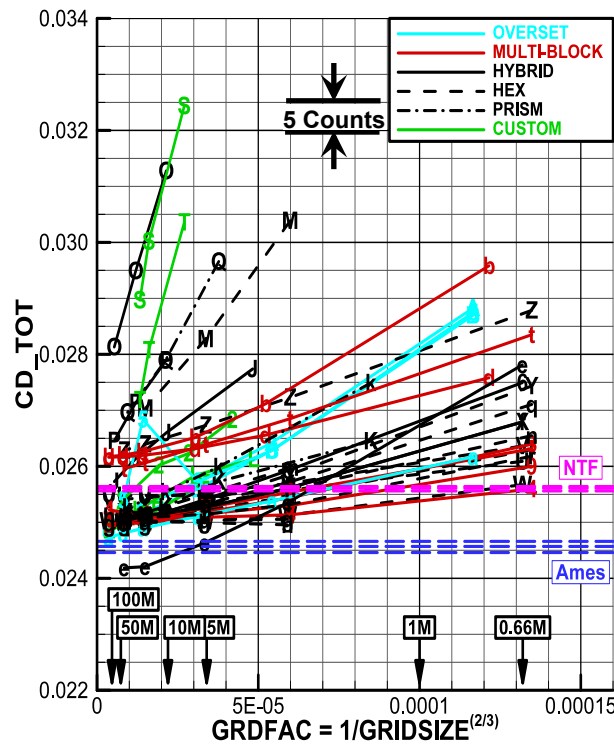


Should we Compare to Wind Tunnel?

Wind Tunnel	CFD
Walls	Free Air
Support System (Sting)	Free Air
Laminar/Turbulent (Tripped)	“Fully” Turbulent (usually)
Aeroelastic Deformation	Rigid 1g Shape
Measurement Uncertainty	Numerical Uncertainty & Error
Corrections for known effects	No Corrections

- Wind Tunnel and CFD measure/compute different things!
- Data are included for reference only!

Case 1: CD_TOT , α , and CM_TOT with Wind Tunnel Results

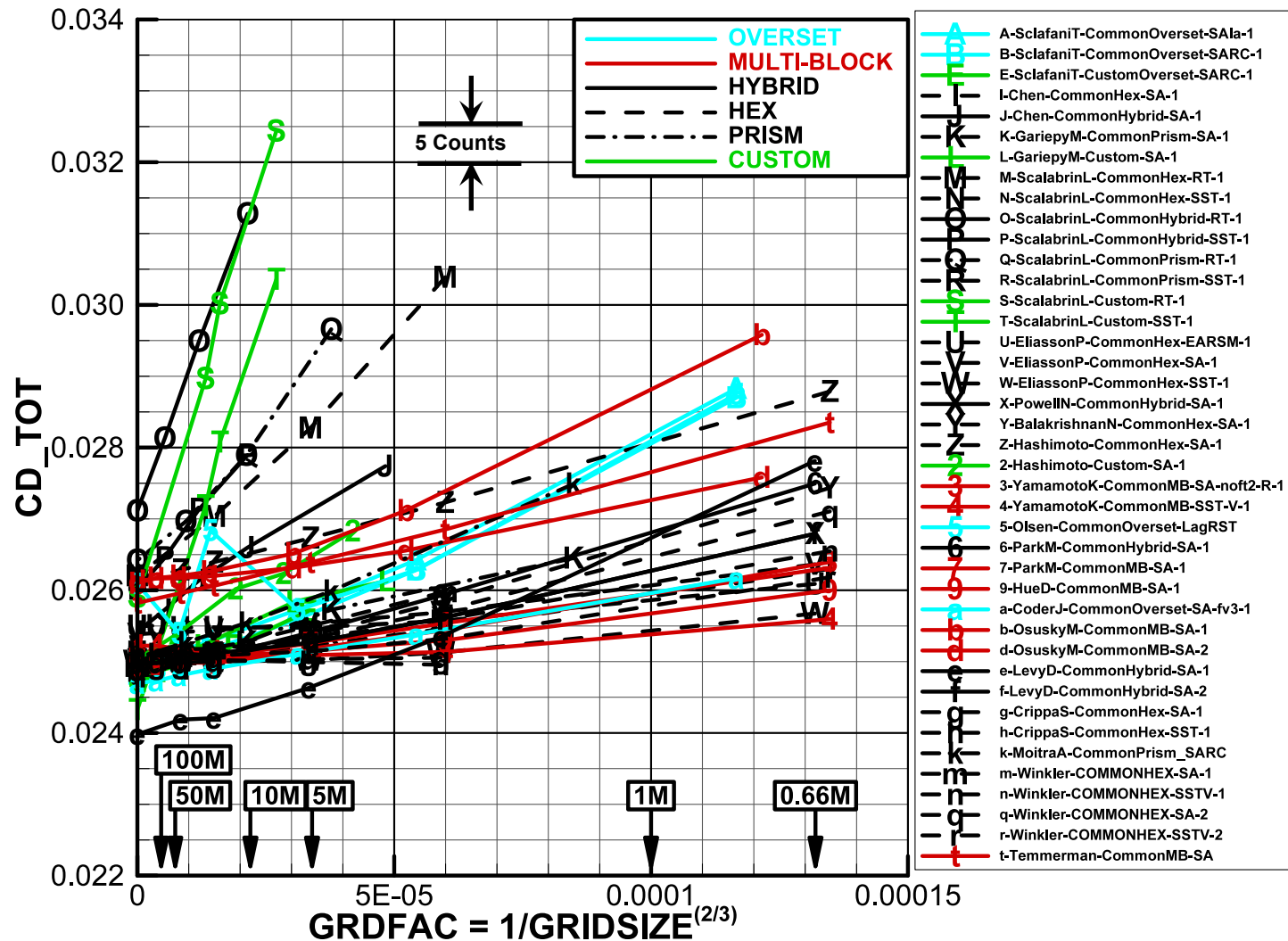


Wind Tunnel Results shown for Reference Only

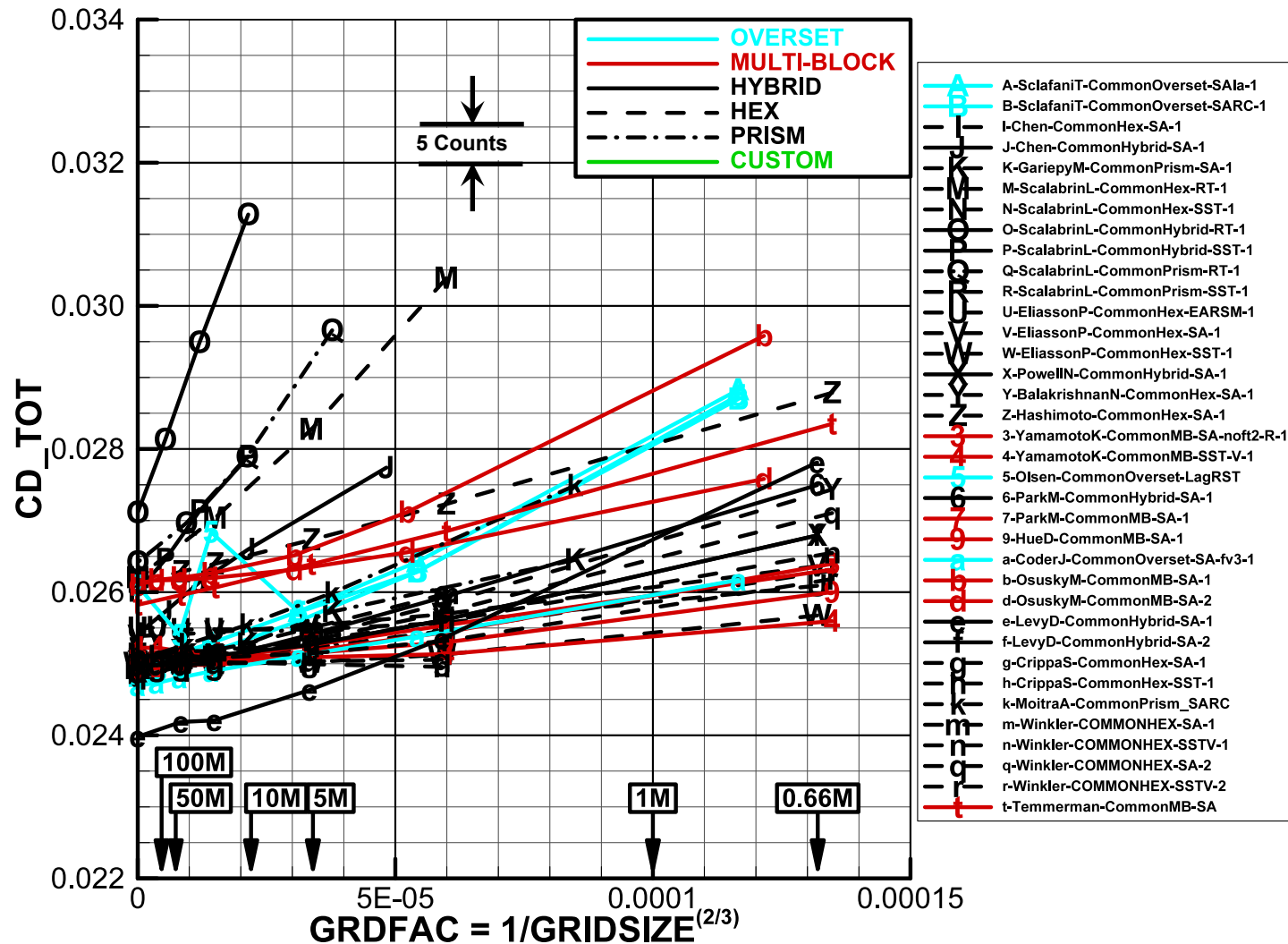
Richardson Extrapolation:

- Standard 2nd order least squares fit (Excel)
- For 2nd order codes, should be linear vs.
 $\text{Grid_Factor} = N^{-2/3}$
- Y-intercept estimates theoretical infinite resolution (continuum) result

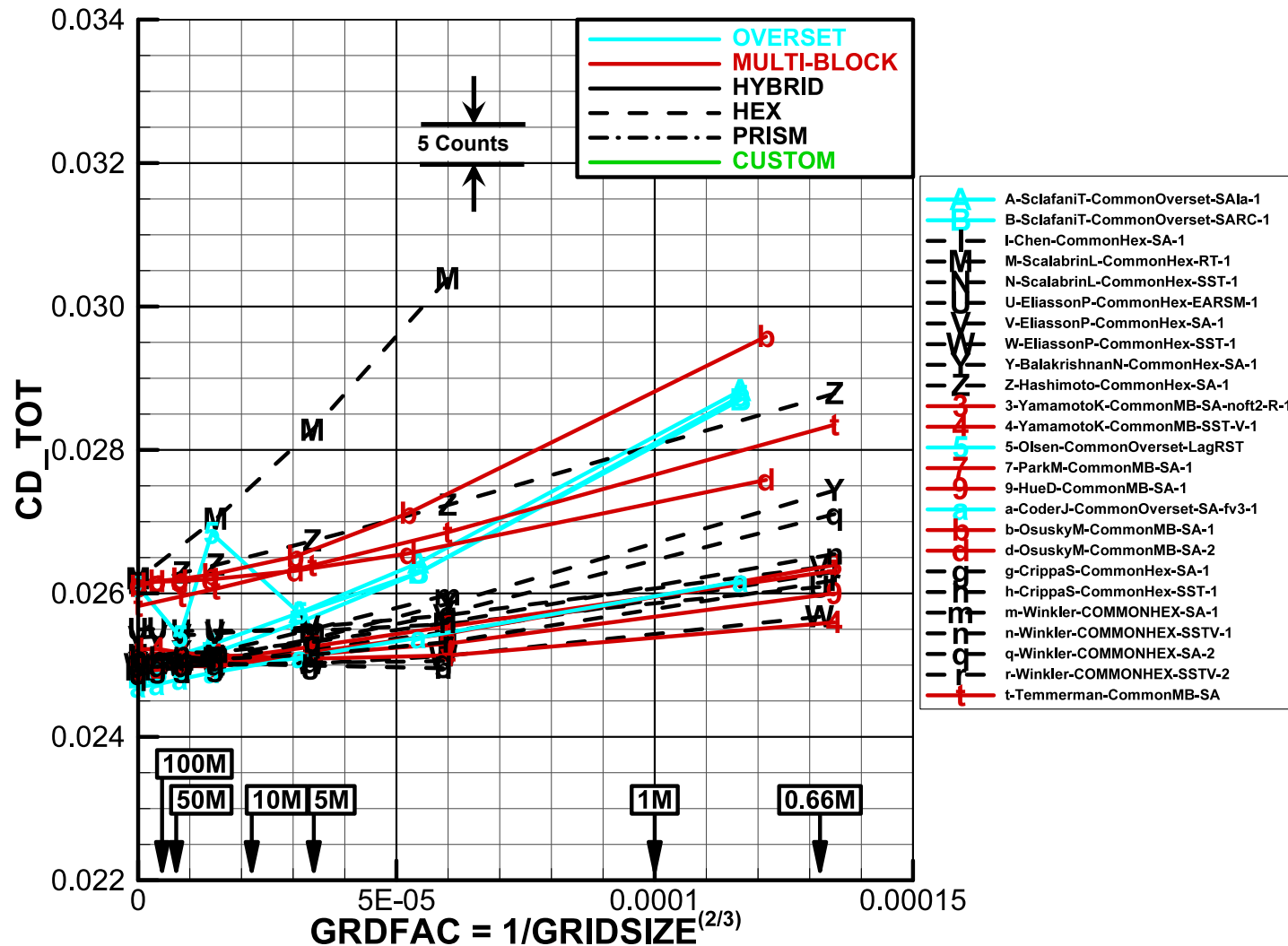
Case 1: Extrapolated CD_TOT by Grid Type



Case 1: Extrapolated CD_TOT by Grid Type (Common Grids Only)



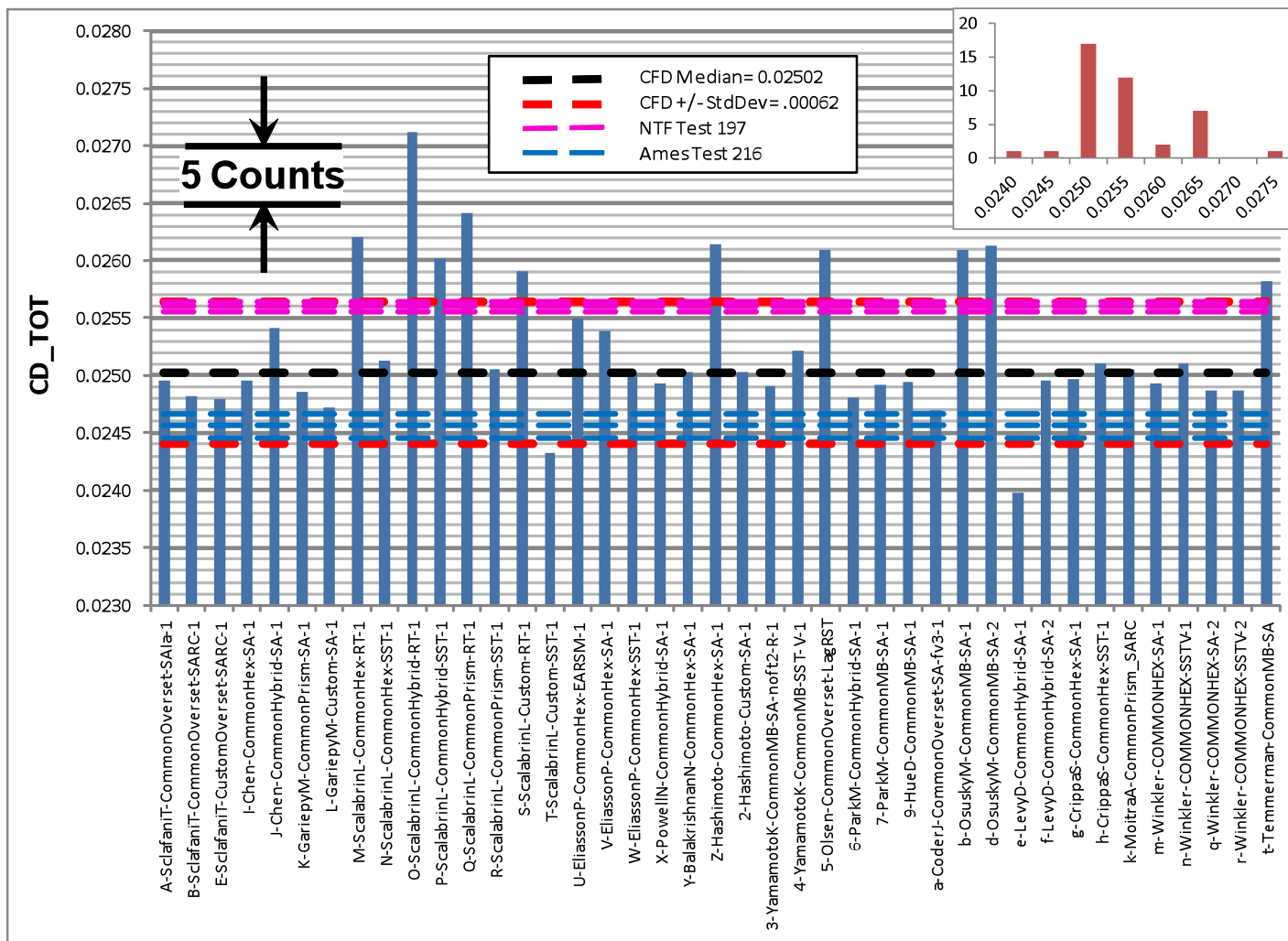
Case 1: Extrapolated CD_TOT by Grid Type (Common Hex Grids Only)



Conclusions from Richardson Extrapolation:

- Most results are monotonically decreasing
- Some are nonlinear
 - Convergence issues
 - Possible flow-feature changes (SOB or TE Separation)
- No clear break-outs with grid type or turbulence model (except for some outliers)
- Scatter is reduced somewhat for Common Grids
 - Scatter still large for coarser grids
 - Best for Hex-based, including Structured, Overset, and Unstructured

Case 1: Extrapolated CD_TOT Statistics



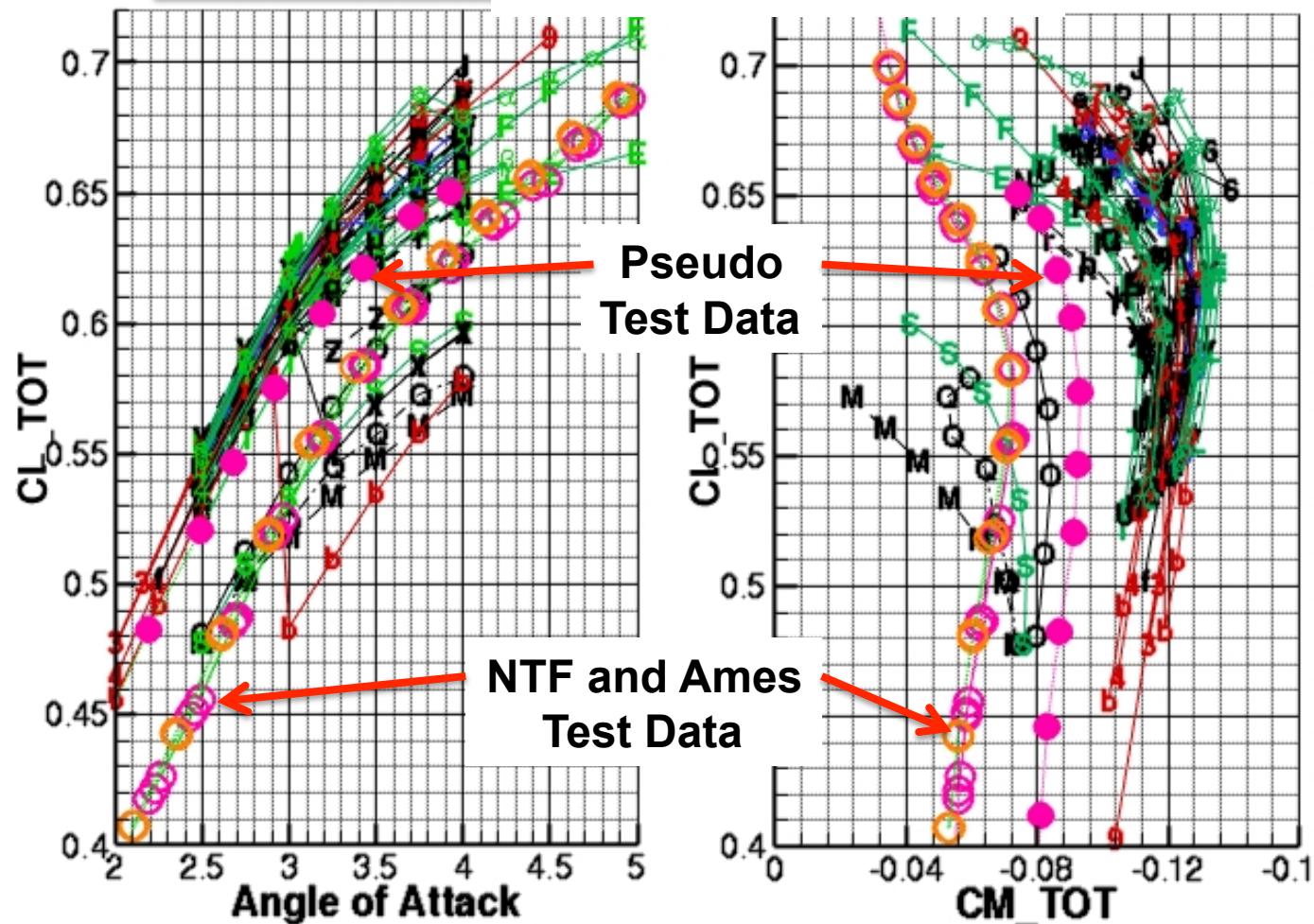
Conclusions from Case 1 Results:

- Still a lot of scatter!
 - Less than DPW4 (was $\sigma=8.1$ for tail on). Are we getting better?
- No clear break-outs with grid type or turbulence model
 - Some Turb. Models are outliers
 - Trends are still hard to isolate due to small sample sizes
- Agreement with experiment on CD_{TOT} is better than for ALPHA and CM_{TOT}
 - Wing aeroelastic effects are likely part of this
 - Spread in CD_{TOT} is similar between wind tunnel and CFD scatter
- Scatter is reduced somewhat for Common Grids
 - Statistics did not change significantly
 - Best for Hex-based, including Structured, Overset, and Unstructured
 - Discretization and Turbulence Modeling is still a major contributor

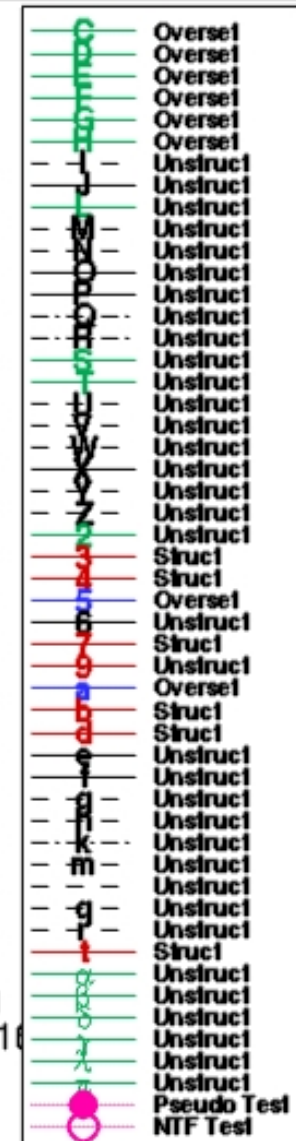
Case 2 Buffet Study:

- NASA Common Research Model, Wing-Body
- Mach=0.85:
 - $\alpha=2.50^\circ, 2.75^\circ, 3.00^\circ, 3.25^\circ, 3.50^\circ, 3.75^\circ, 4.00^\circ$
- Grid Resolution Level:
 - 3) Medium,
- Chord Reynolds Number: 5×10^6

Case 2 – All Solutions

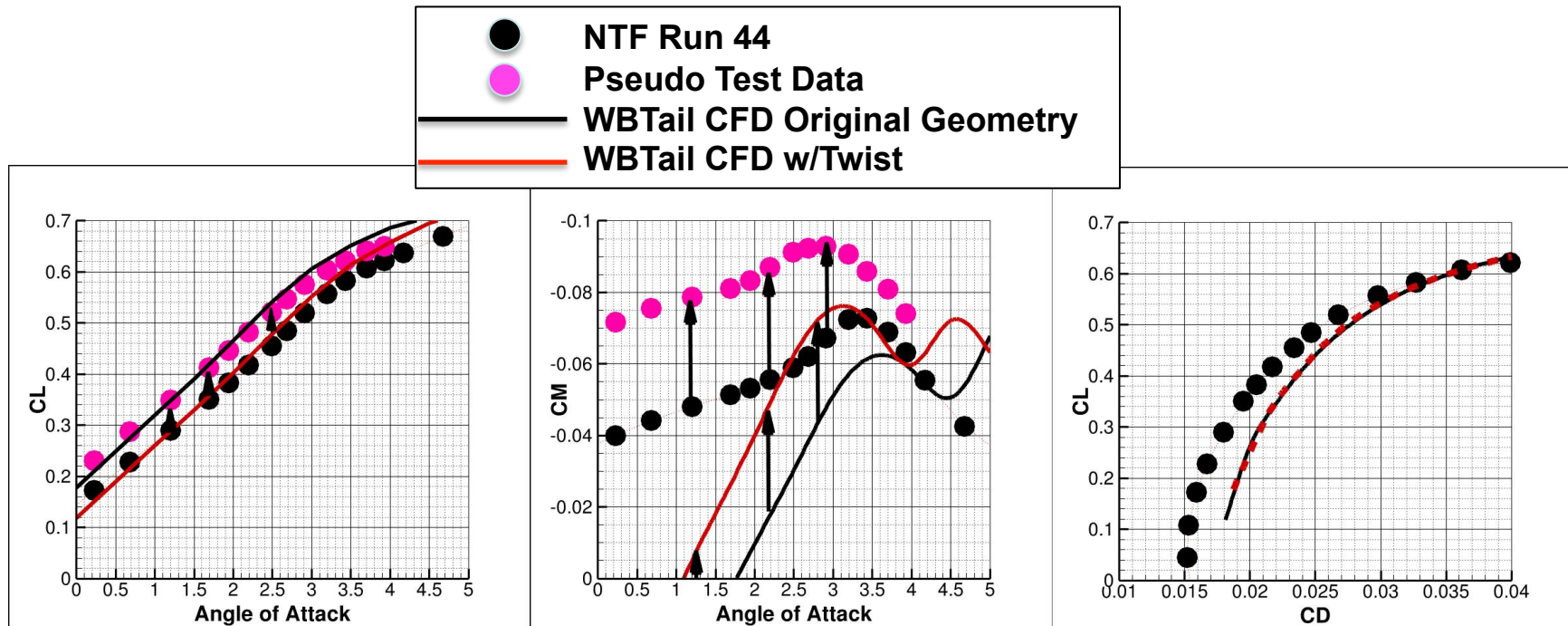


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209



CREATION OF “PSEUDO TEST DATA”

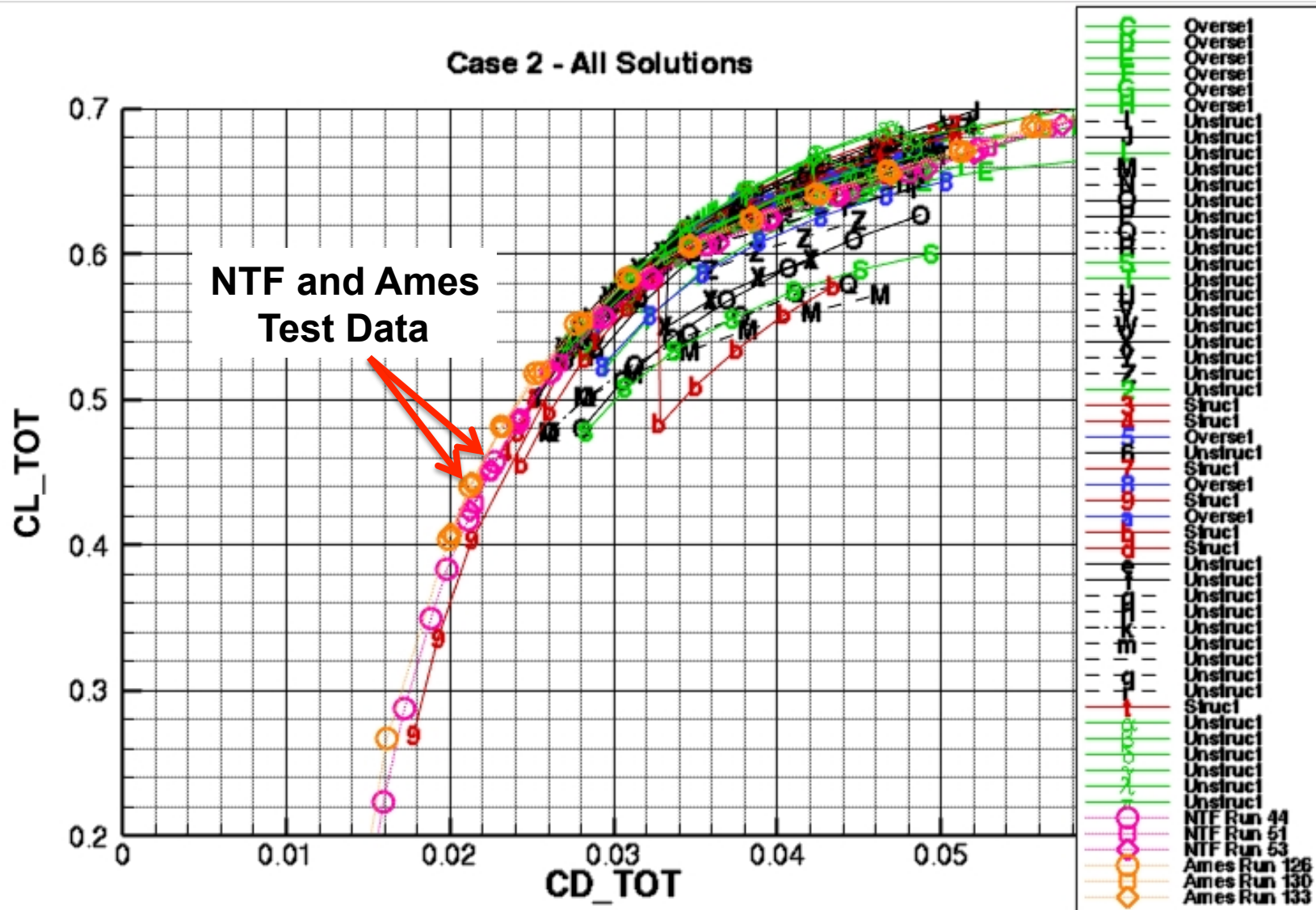
- The CRM geometry used for DPW5 was that of the wind tunnel model definition
- AIAA-2012-3209 details recent CFD analyses to account for the wing aeroelastic twist at Mach=0.85, $CL=0.50$, and for additional wind tunnel mounting system effects.
- “Pseudo Test Data” were created from the NTF data and CFD analyses to reflect what the test data might look like for the wing without the “ $CL=0.50$ aeroelastic” twist.



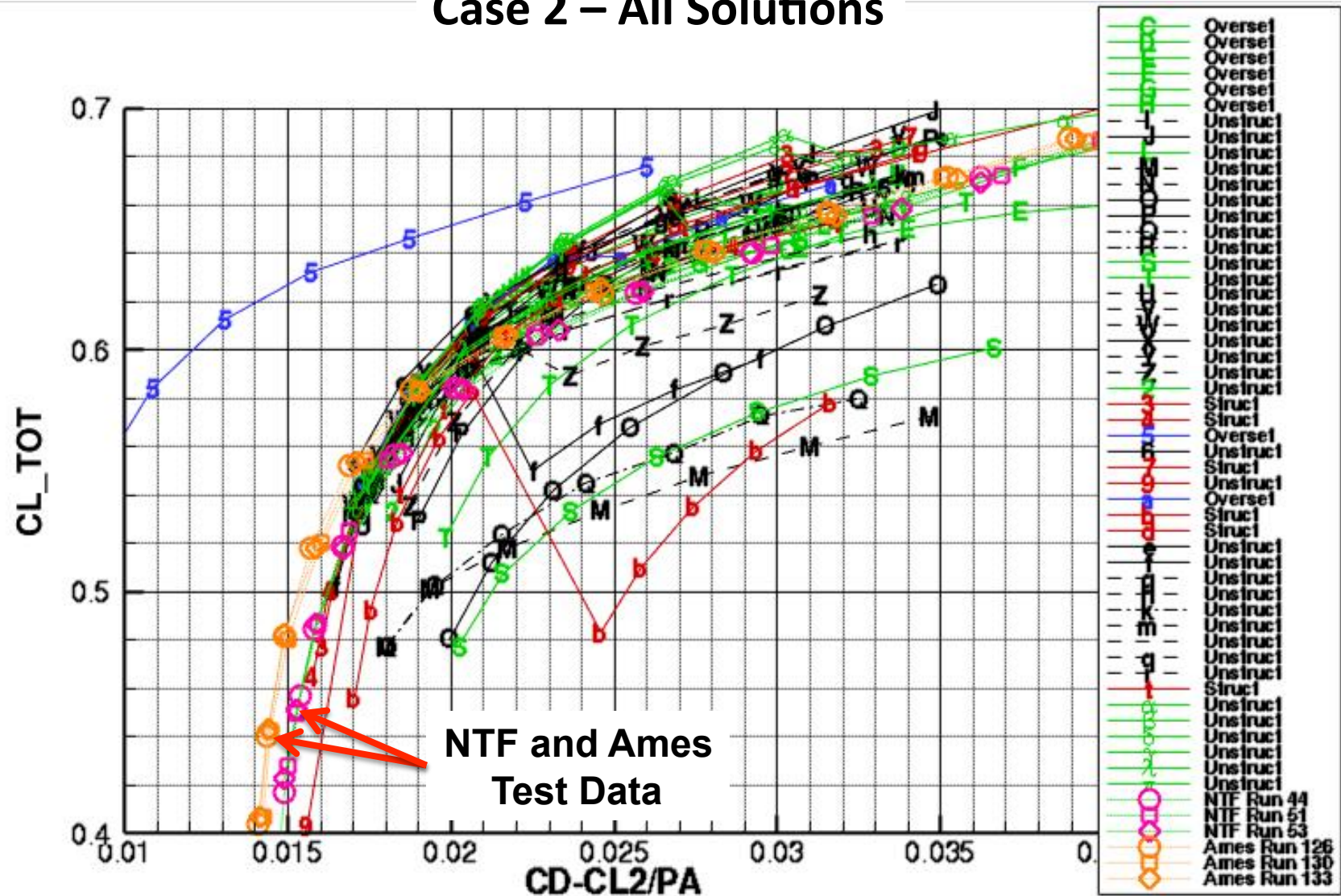
- No corrections were applied to drag data

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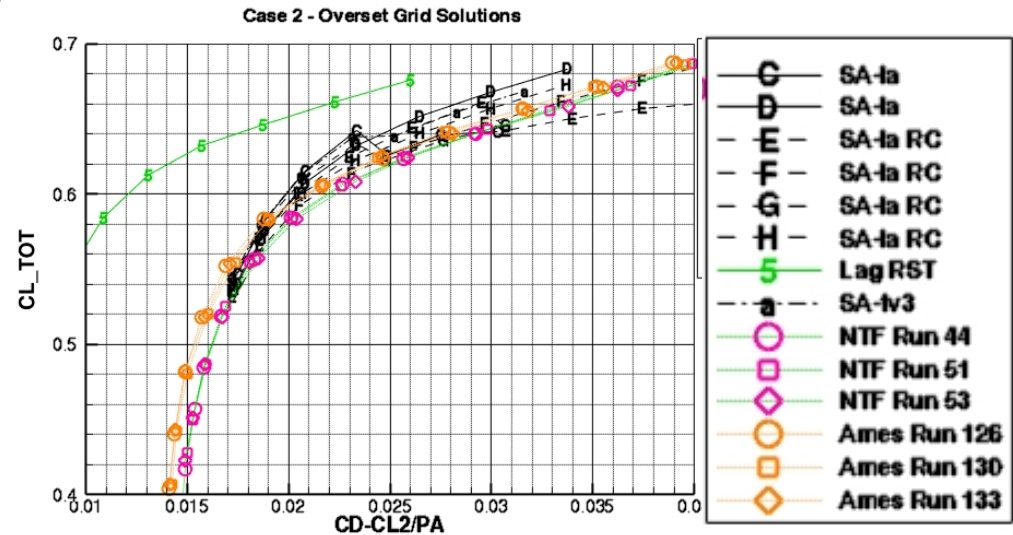
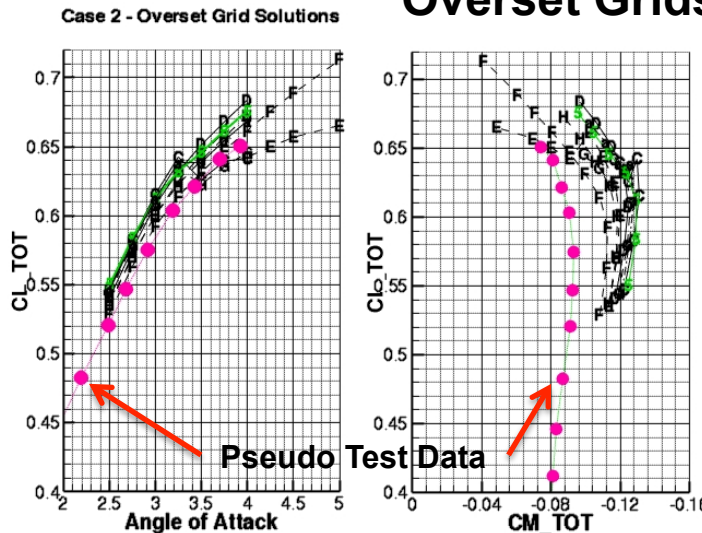
Case 2 – All Solutions



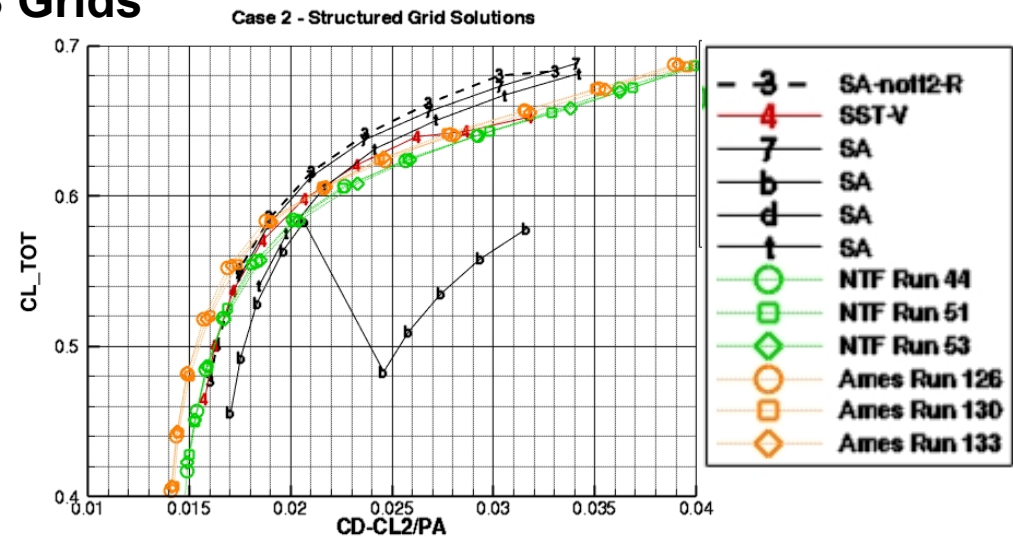
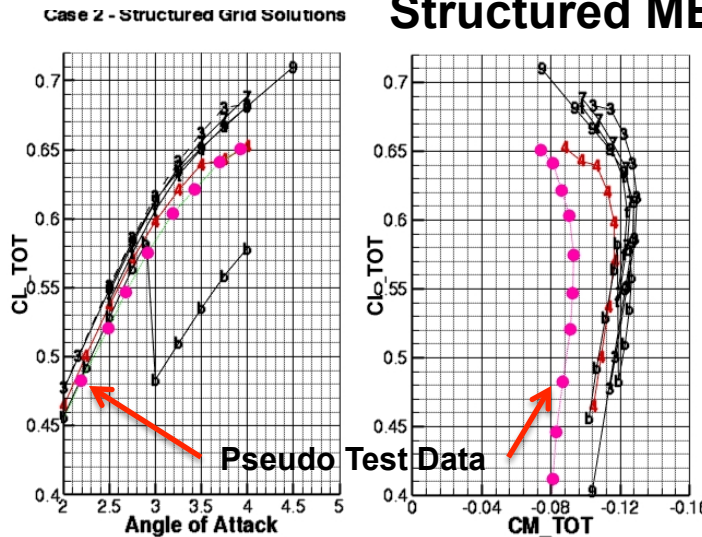
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Overset Grids



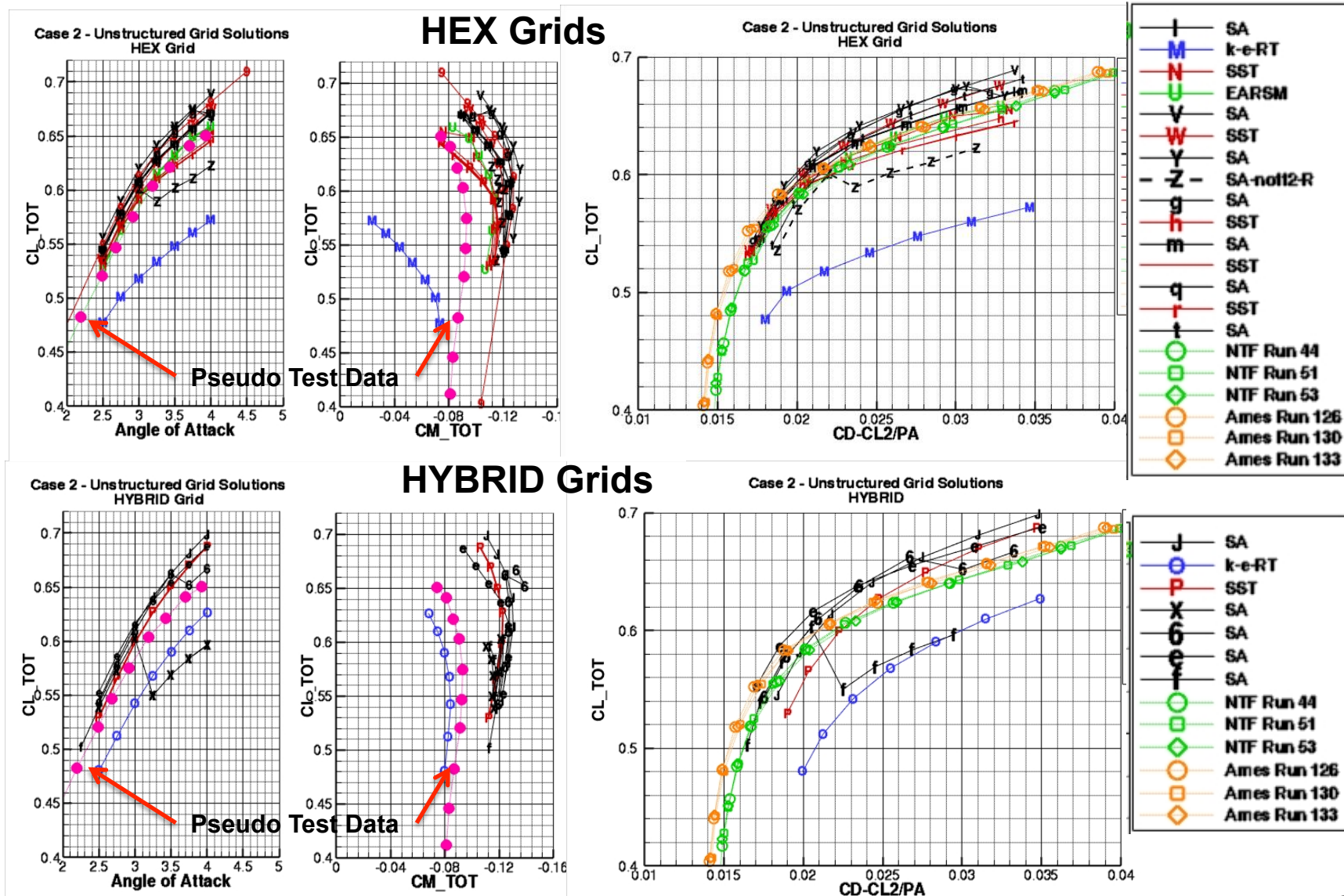
Structured MB Grids



Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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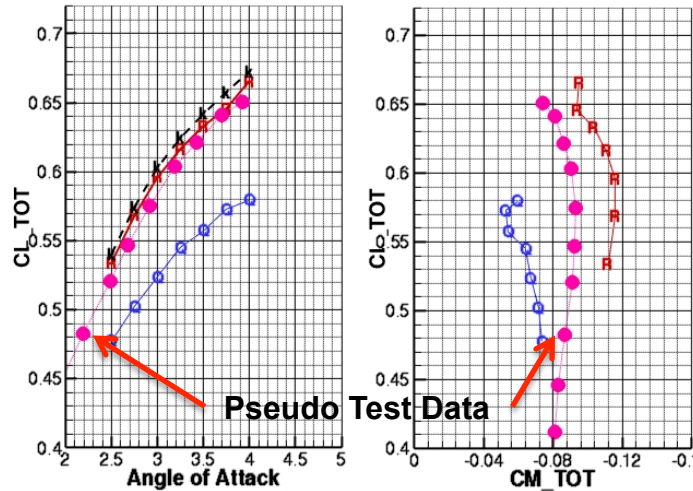
Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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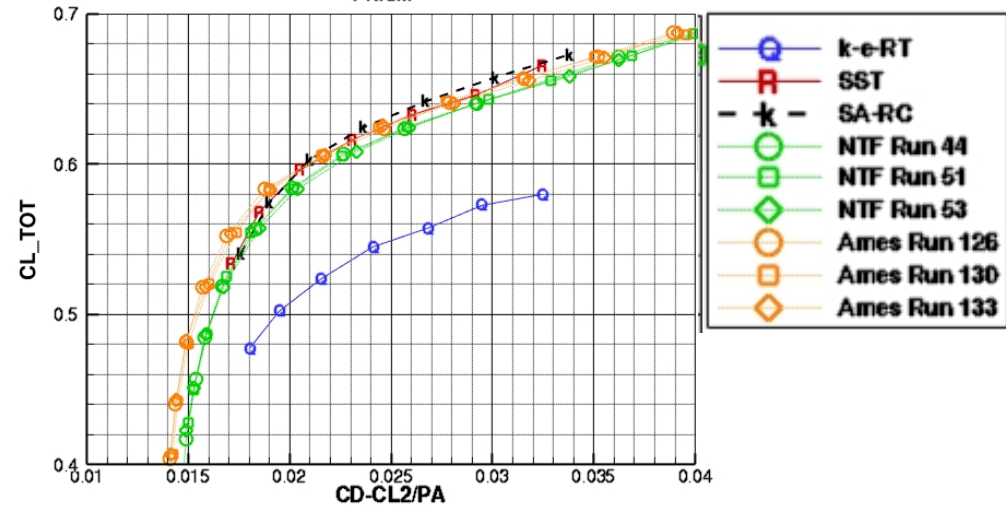
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PRISIM Grids

Case 2 - Unstructured Grid Solutions
Prism Grid

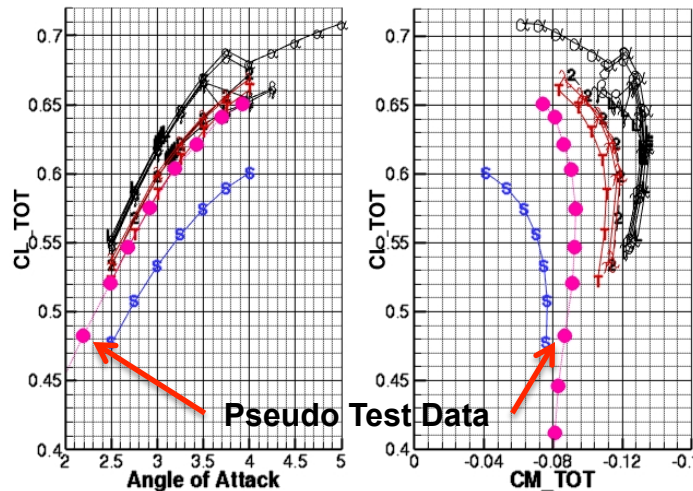


Case 2 - Unstructured Grid Solutions
PRISM

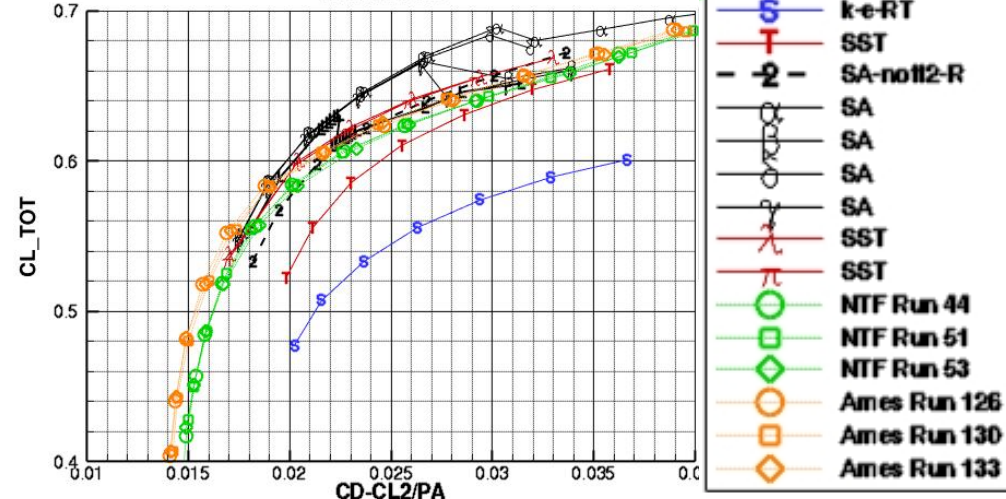


Custom Unstructured Grids

Case 2 - Unstructured Grid Sol
Custom Grids



2 - Unstructured Grid Solutions
Custom Grids

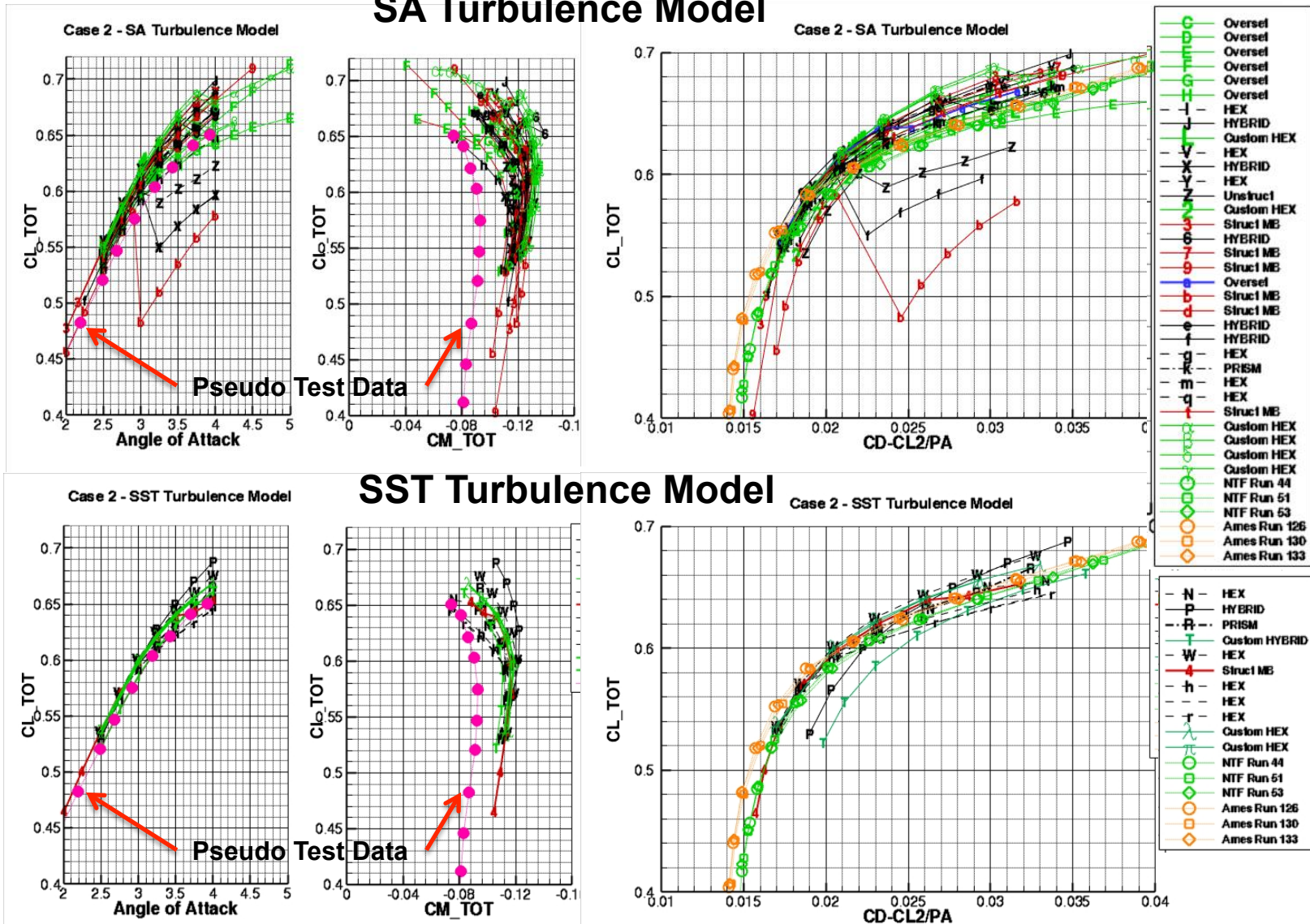


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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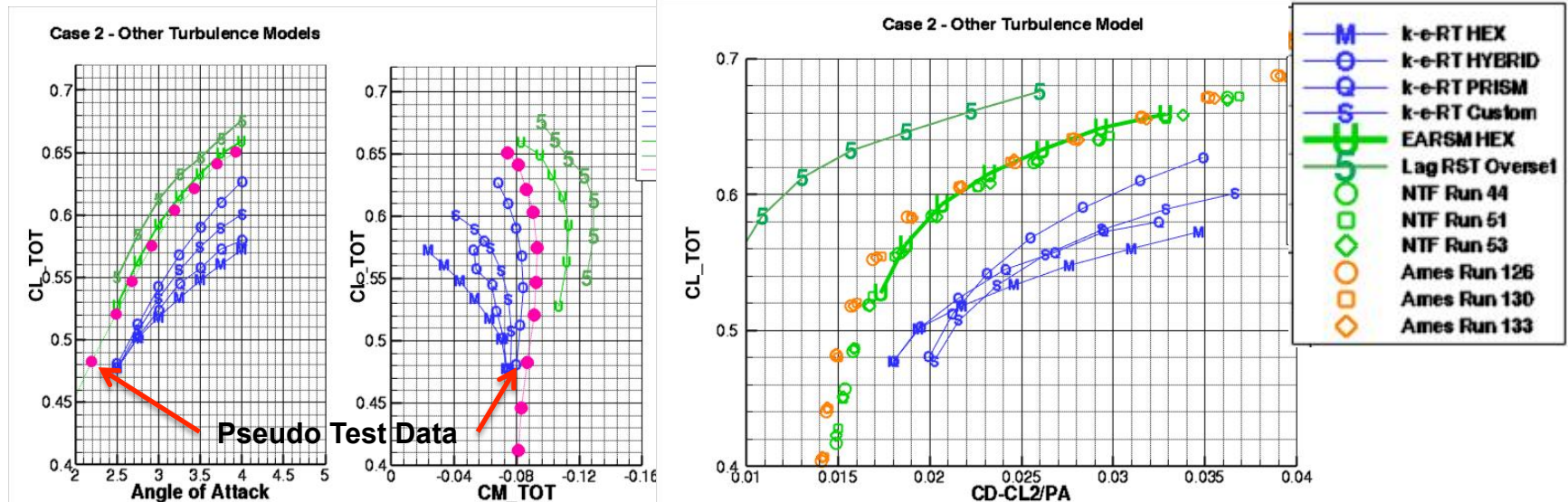
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SA Turbulence Model



Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

Other Turbulence Models

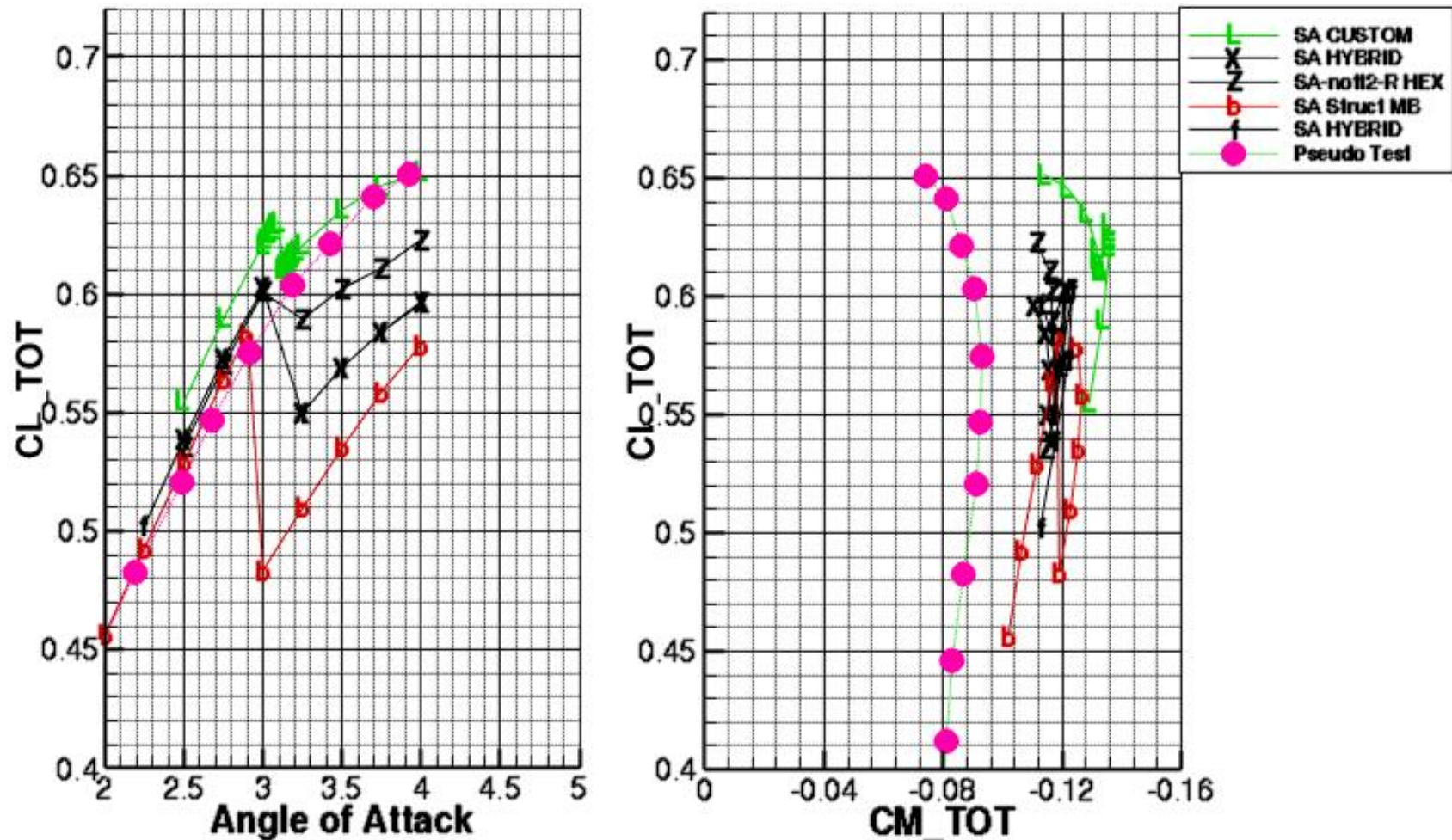


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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Case 2 - CL Break AoA=3.0 or Lower

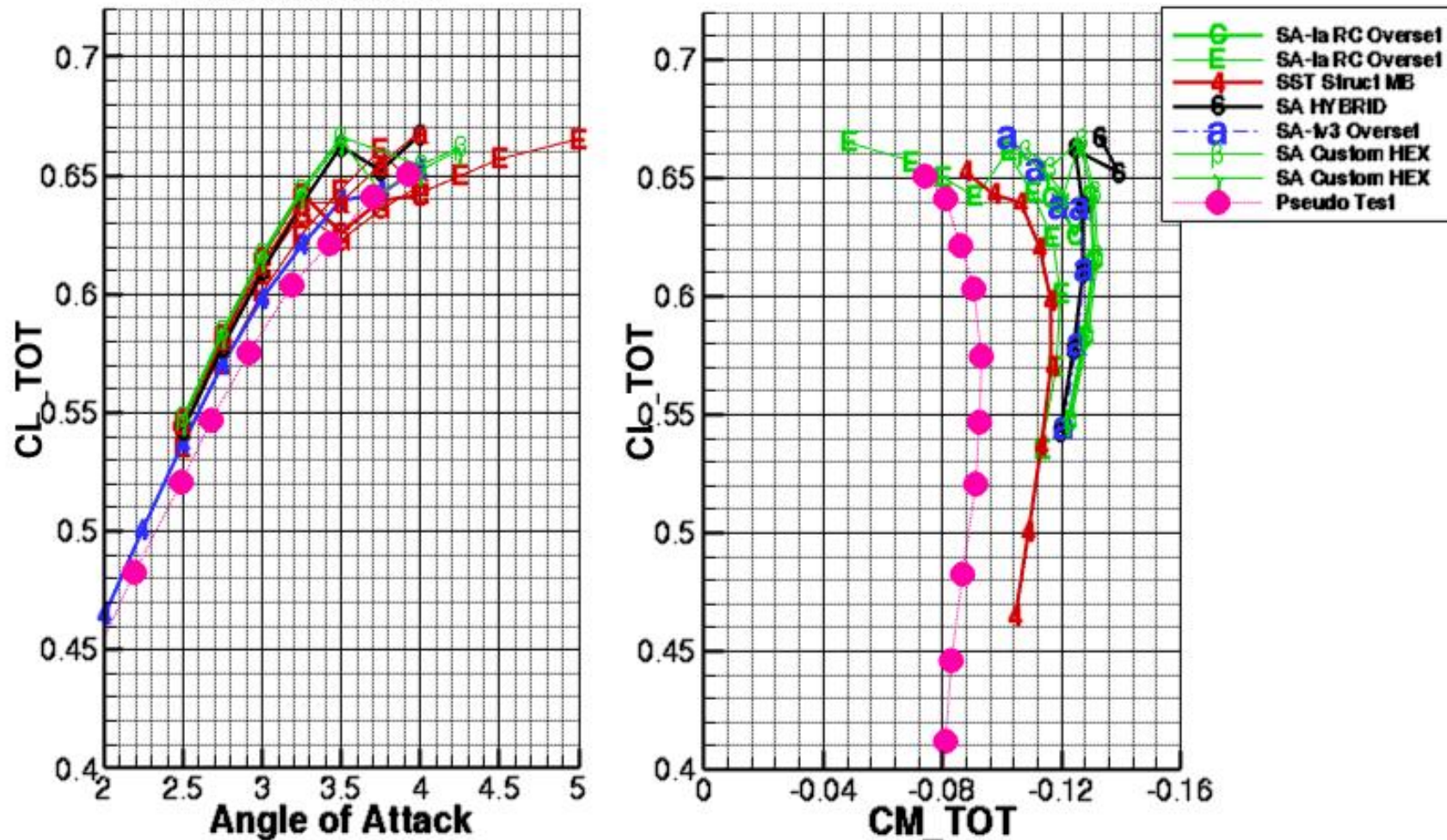


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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Case 2 - CL Break between
AoA=3.25 to 3.75

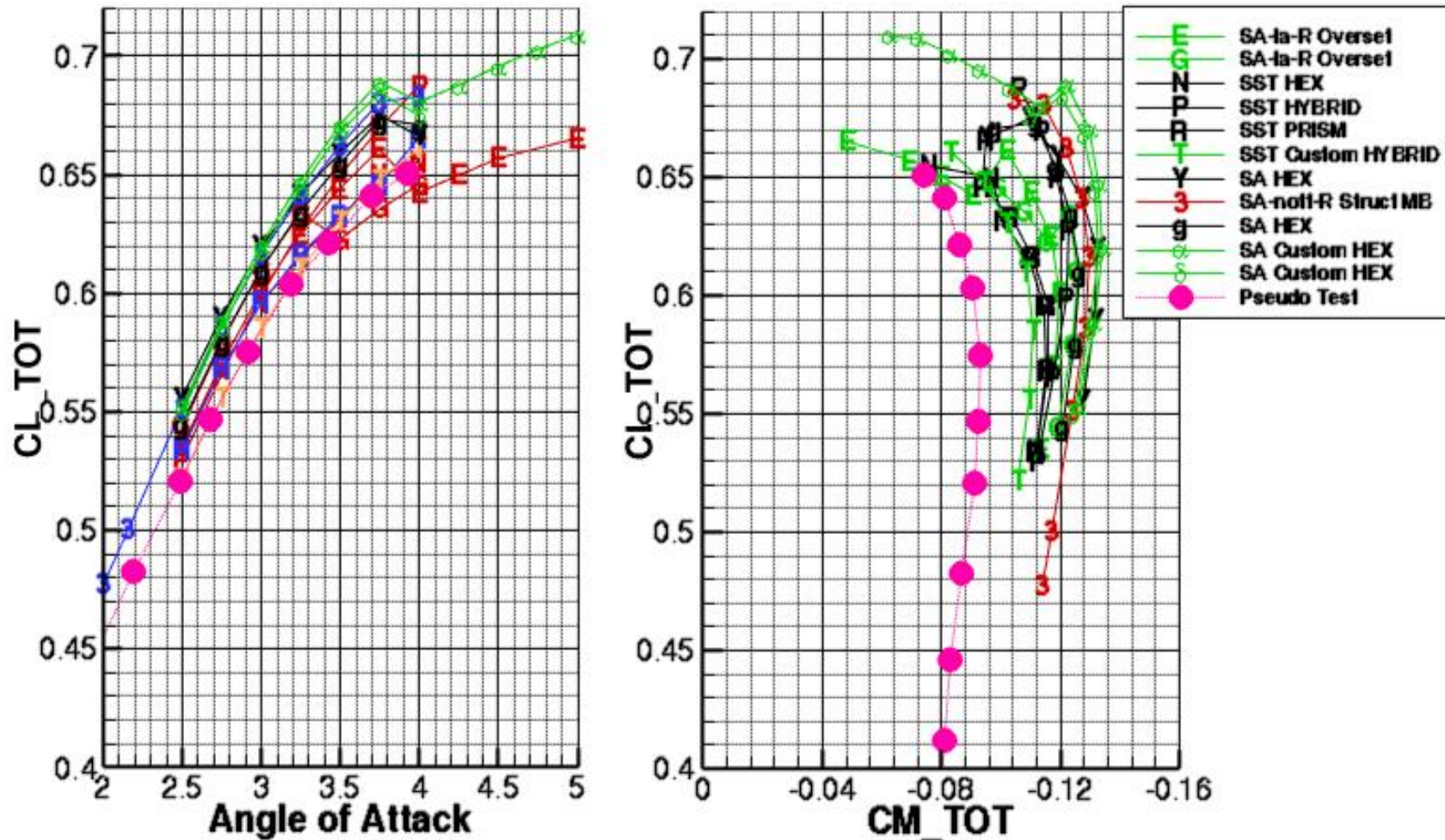


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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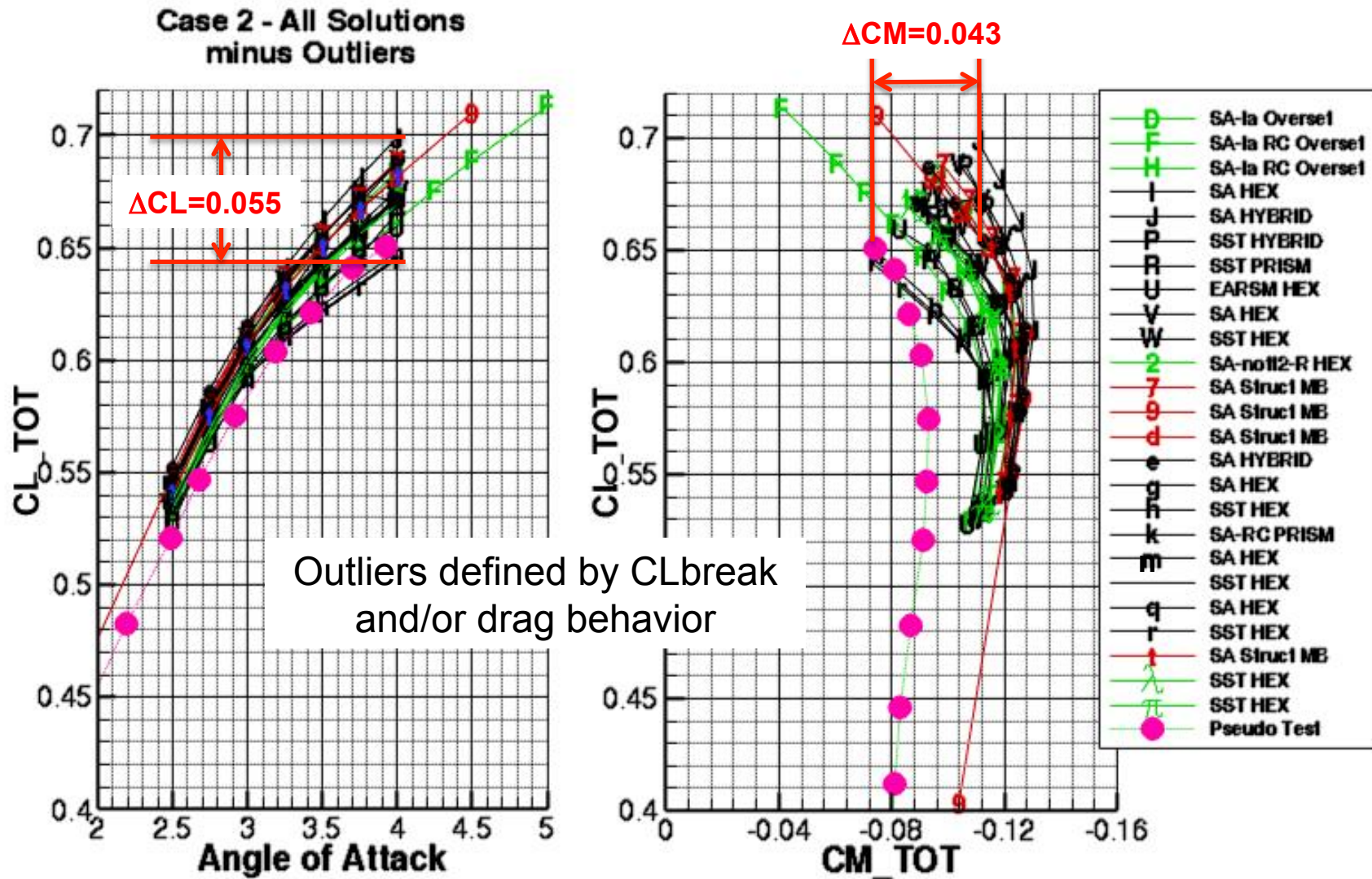
Case 2 - CL Break AoA=3.75



Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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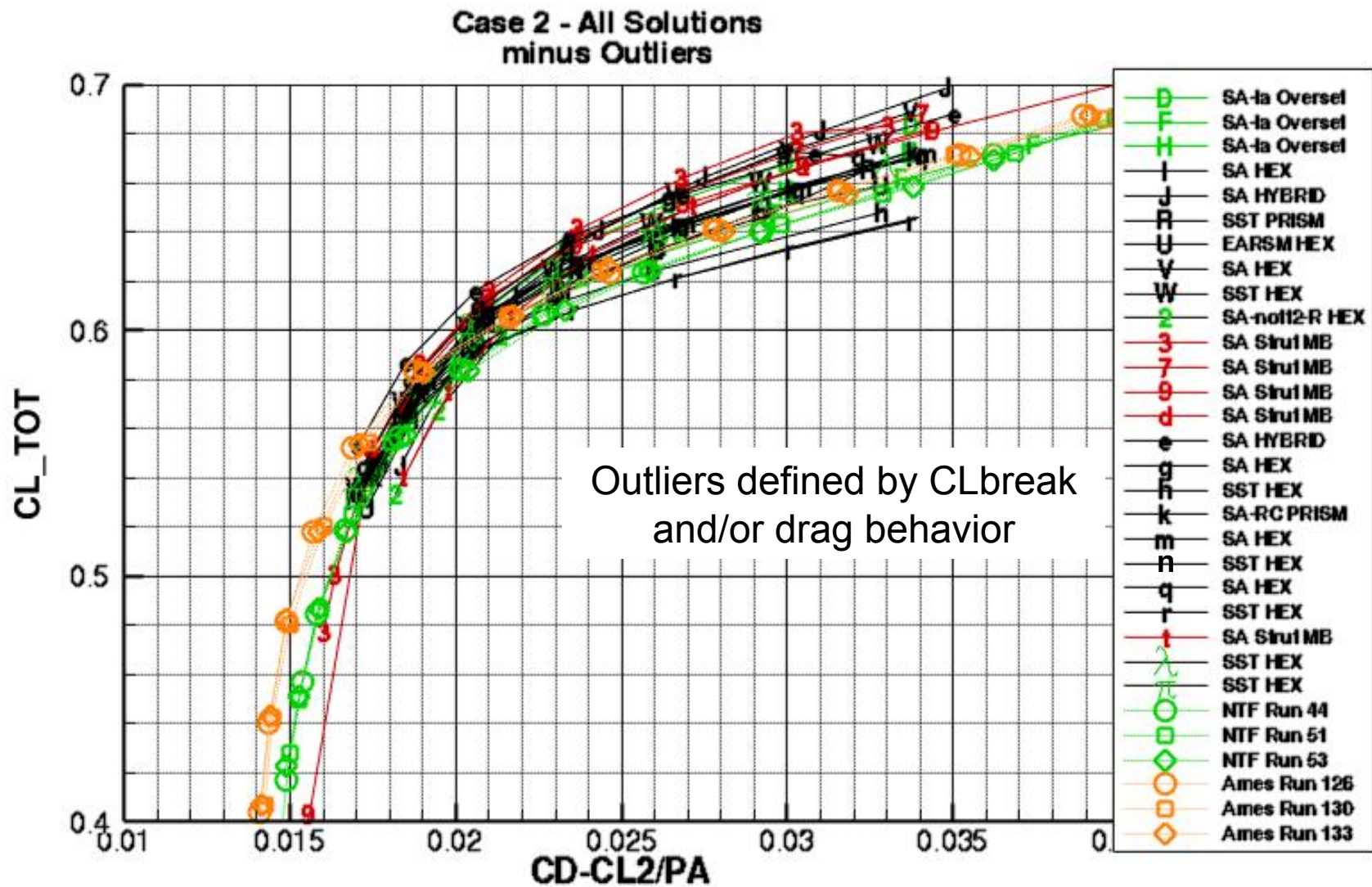
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Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

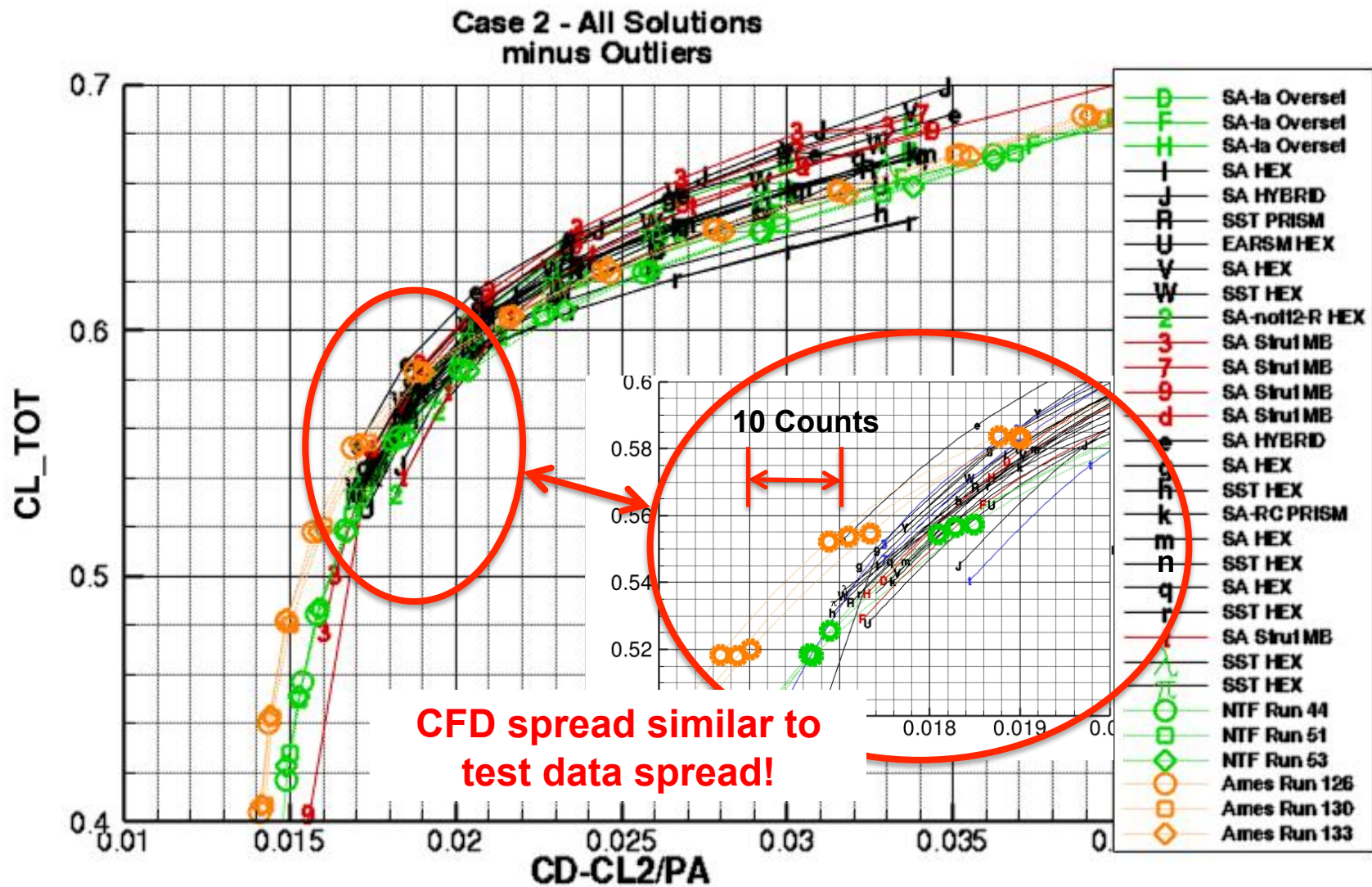
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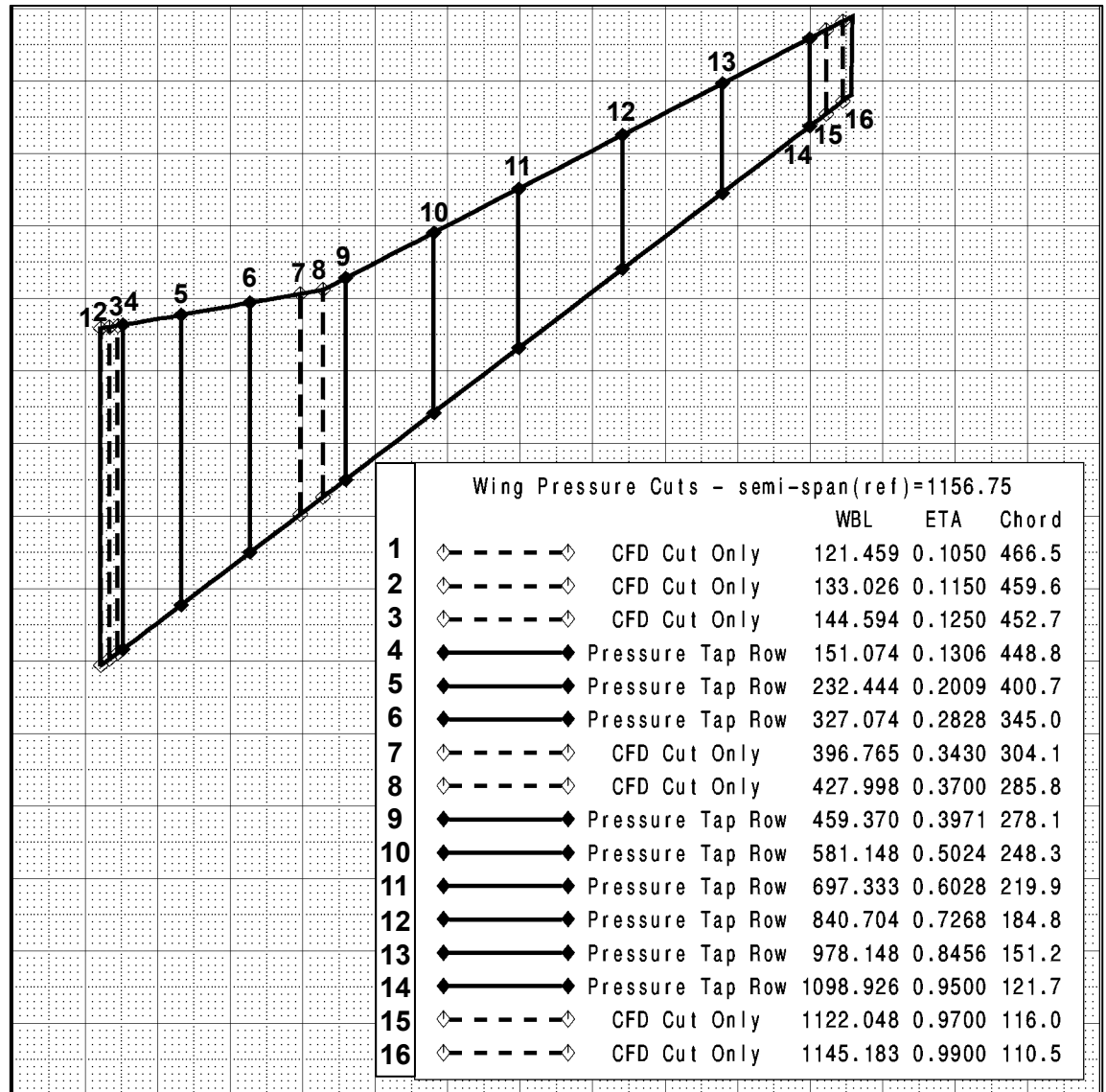
Case 2 - Concluding Remarks

- No clear break-outs with grid type or turbulence model (except for some outliers)
- In general, the k-e-RT and Lag RST results tend outside the norm of the other solutions.
- For all solutions minus outliers
 - Relatively tight forces and moment at $\alpha=2.5^\circ$
 - Significant force and moment spread at $\alpha=4.0^\circ$ $\Delta CL=0.055$, $\Delta CM=0.043$
- CM predicted too negative – is it CFD, test, geometry, etc.?
- Steady aeroelastic effects are significant
 - Must be included in CFD to better assess accuracy
- Wing section characteristics (section CL, CM) needed to better assess CFD
- High angles of attack characterized by significant shock induced separation
 - How steady is the real flow at these conditions? Need dynamic test data?
 - If there is a significant amount of flow unsteadiness at high angles of attack is RANS adequate or do we need URANS or DES?

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Pressure Data



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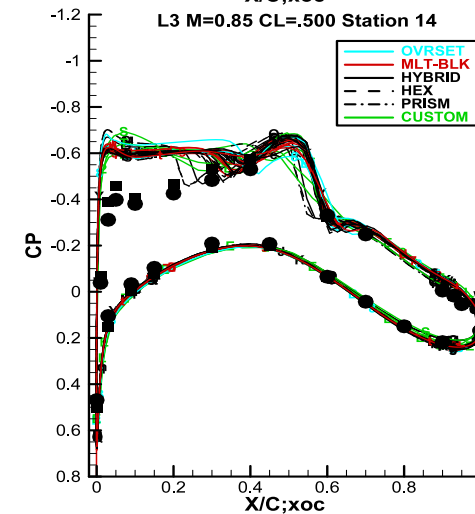
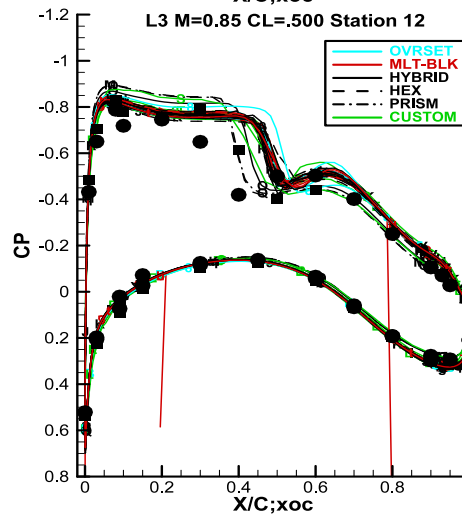
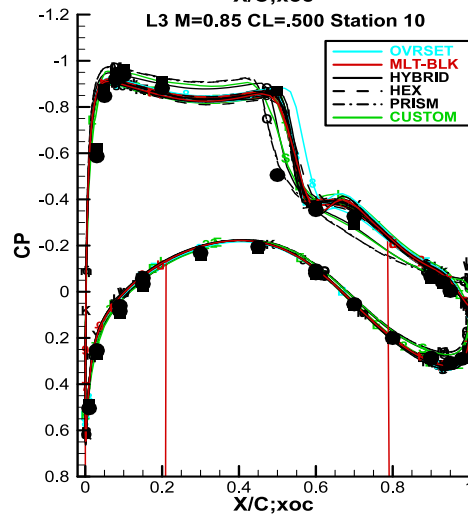
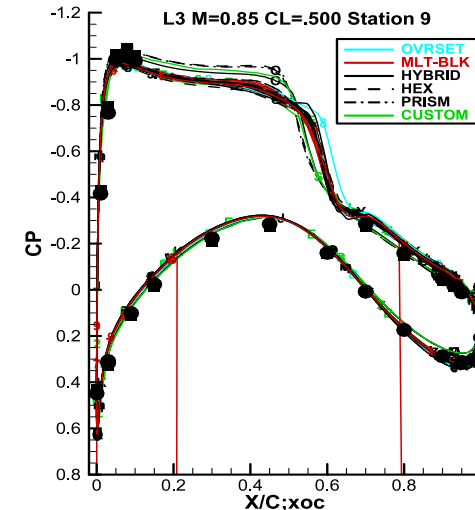
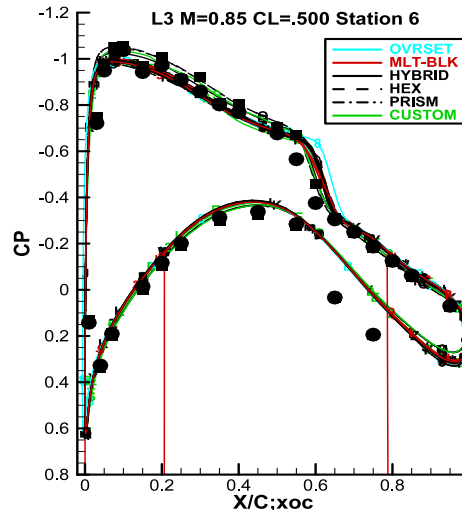
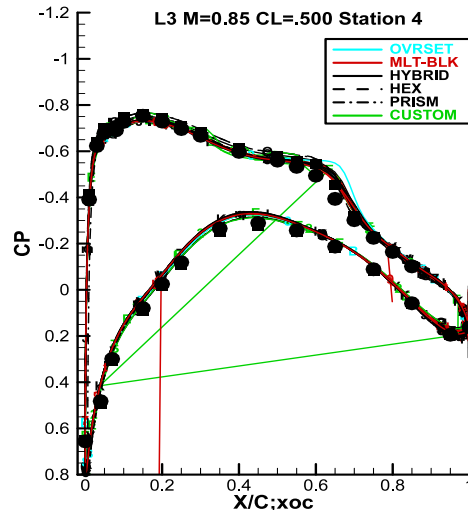
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Case 1: Level 3 Grid, $M=0.85$, $C_L=.50$ Spanwise Variation

NTF Test 197 Run 44:

● $\alpha=2.68^\circ$, $C_L=0.485$

■ $\alpha=2.91^\circ$, $C_L=0.519$

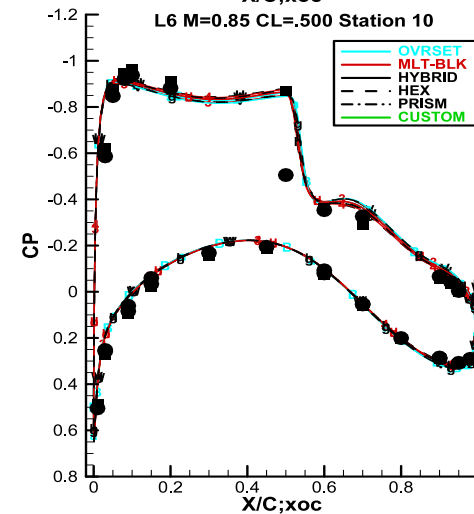
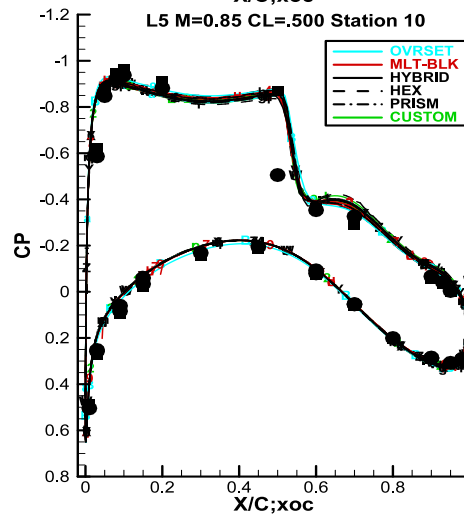
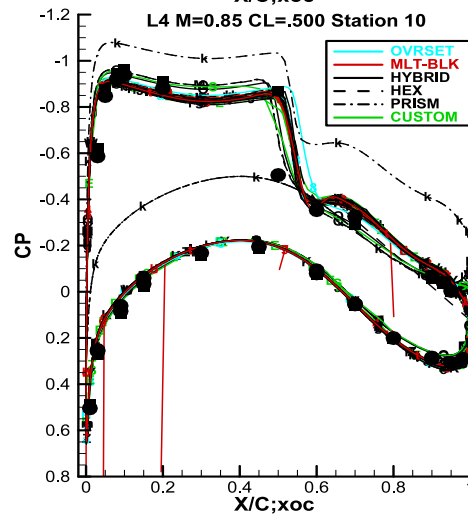
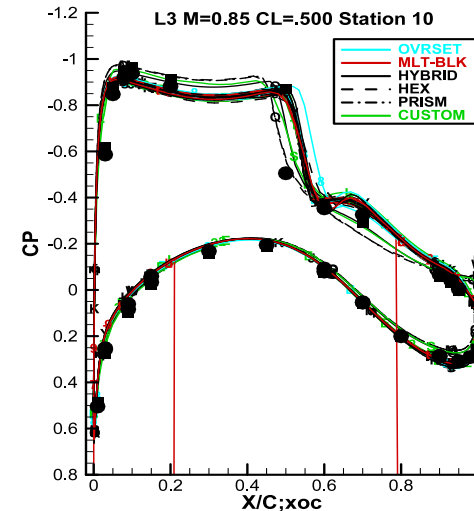
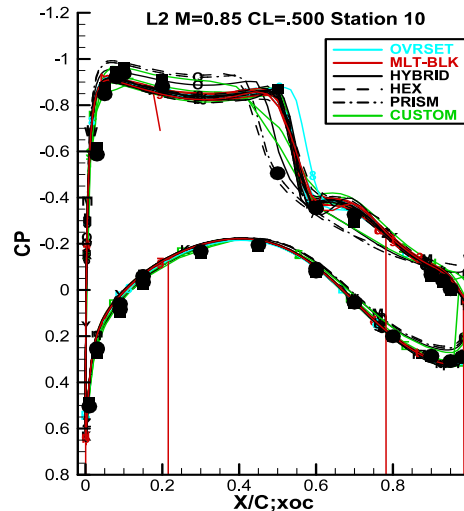
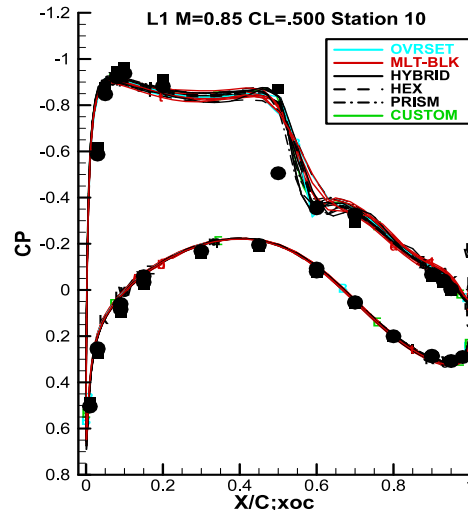


Case 1: Grid Refinement Study, $M=0.85$, $C_L=.50$ Station 10, $\eta=.502$

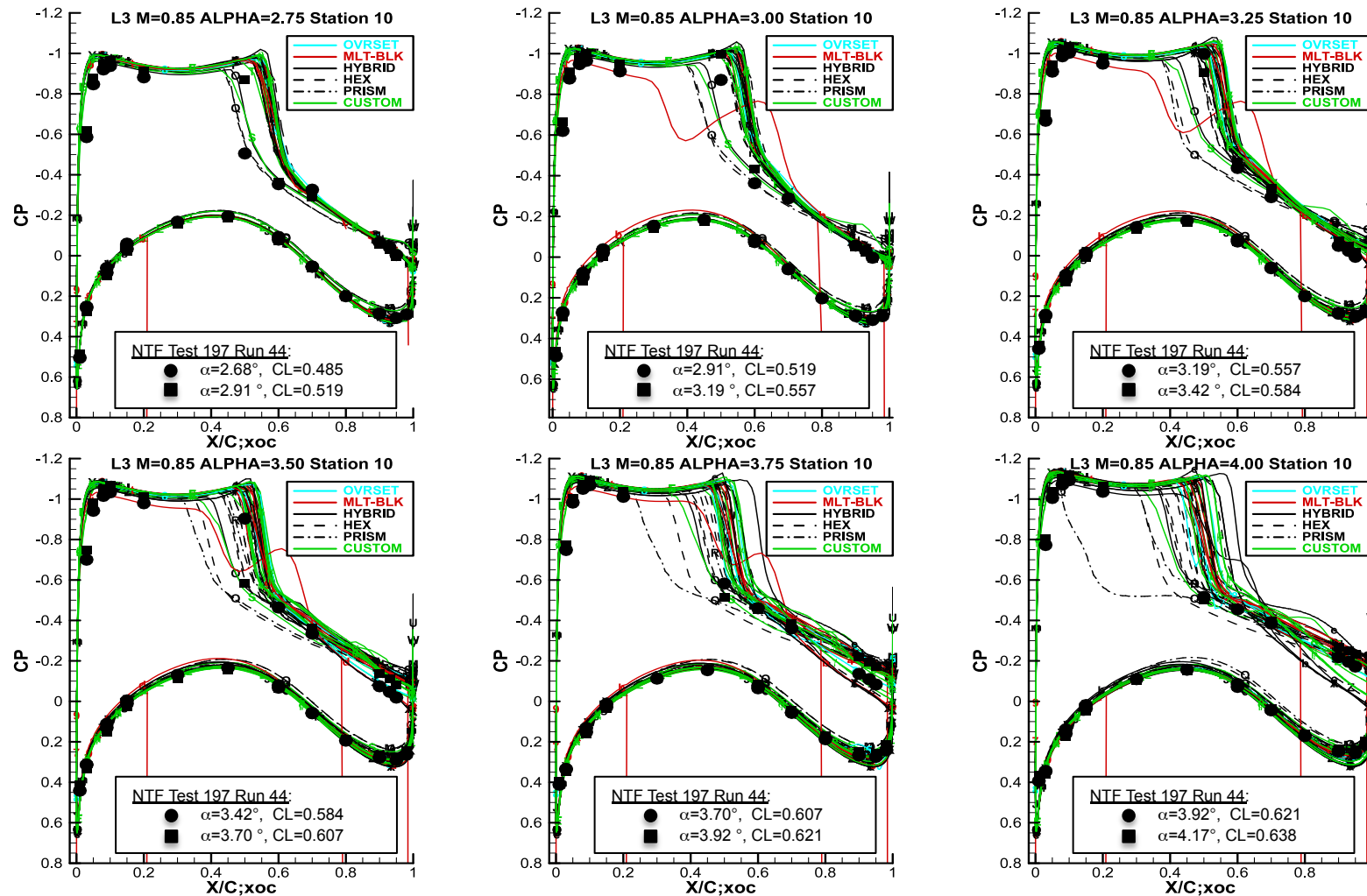
NTF Test 197 Run 44:

● $\alpha=2.68^\circ$, $CL=0.485$

■ $\alpha=2.91^\circ$, $CL=0.519$



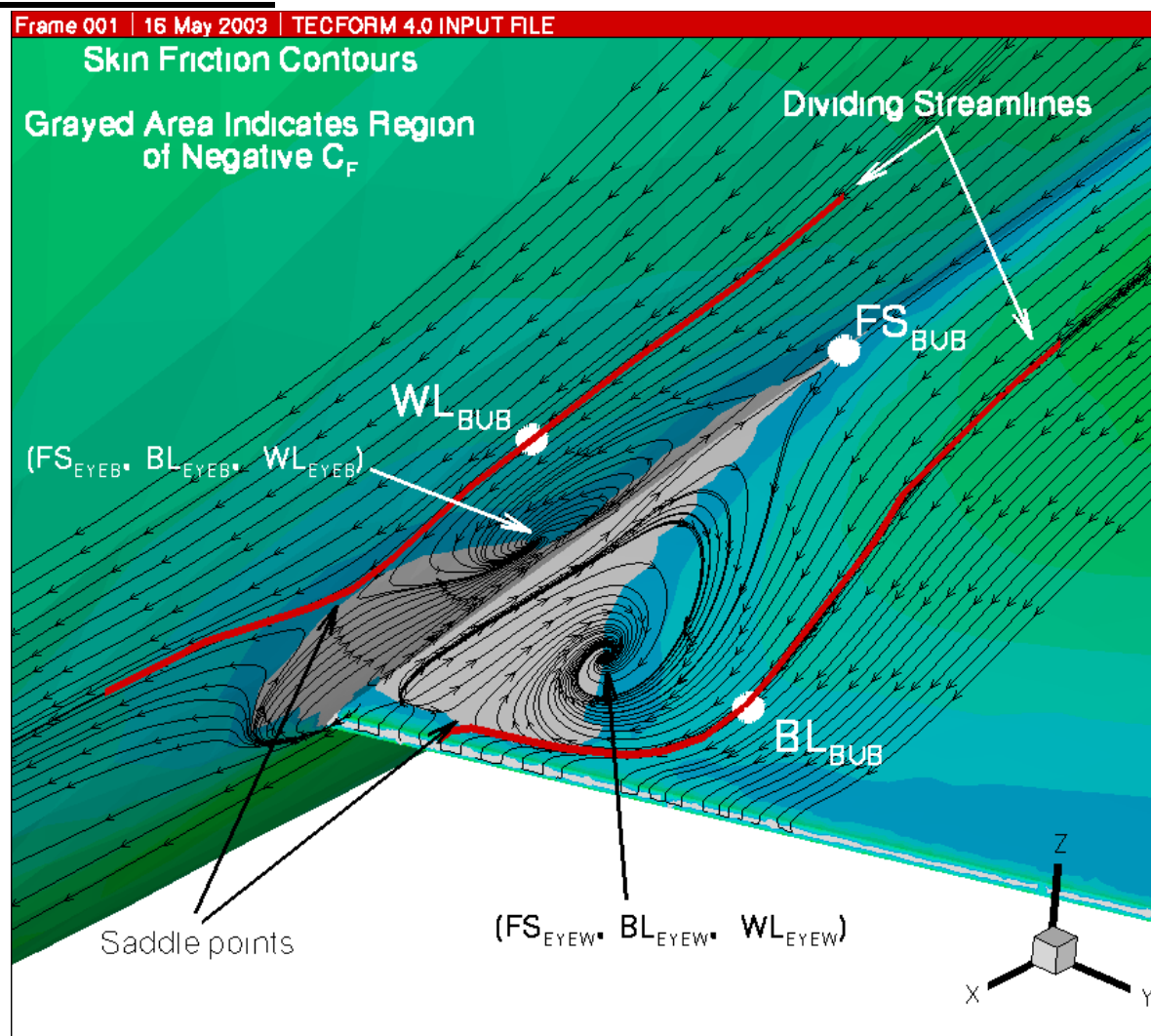
Case 2: Buffet Study, Level 3 Grids, $M=0.85$ Station 10, $\eta=.502$



Conclusions from Pressure Data:

- Agreement with experiment deteriorates at outboard stations, likely due to aeroelastic effects
- Variations with grid level hard to discern due to reduced number of data sets
- Variation at high alphas due to separation effects on shock location
- No clear break-out with grid type (Turbulence model affects not examined yet)

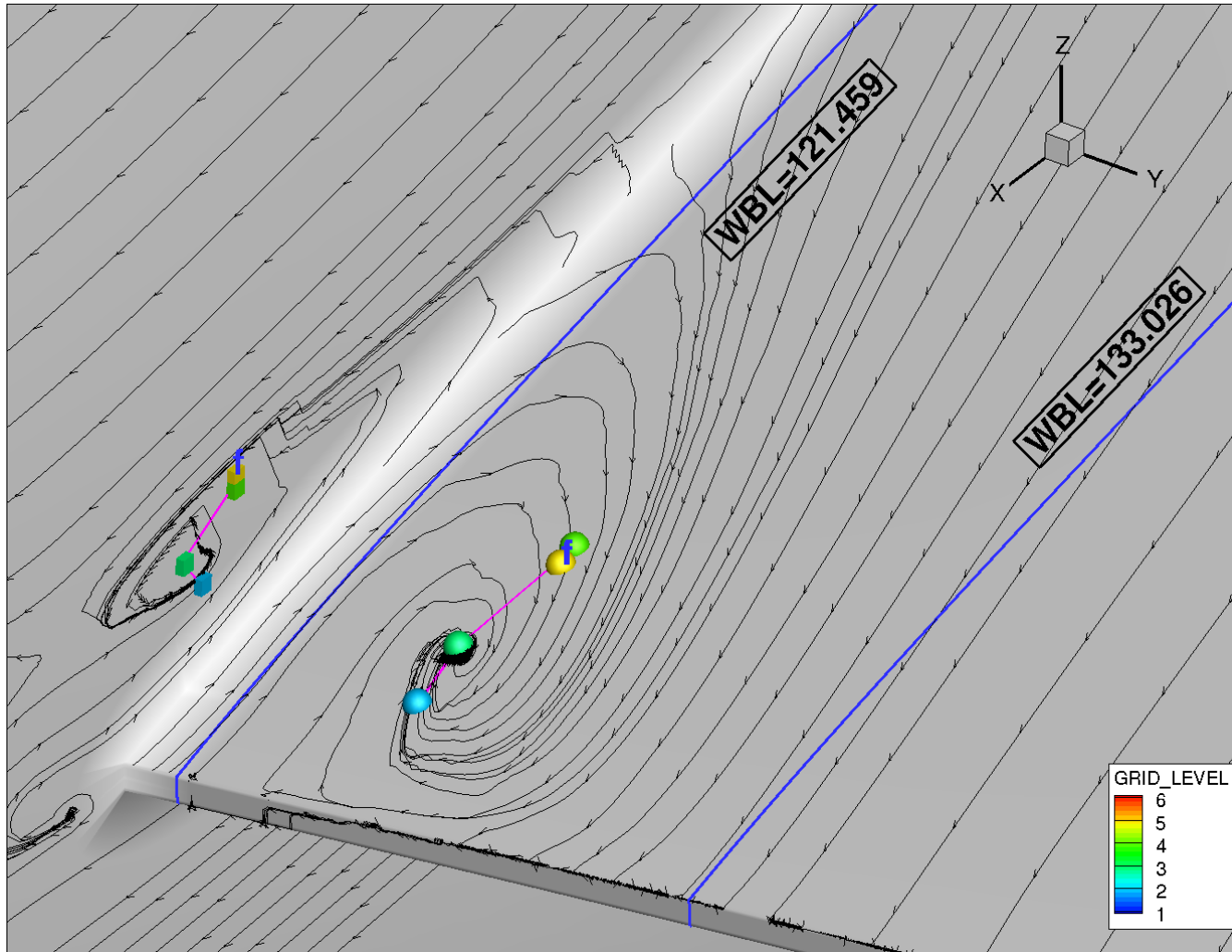
Separation Bubble



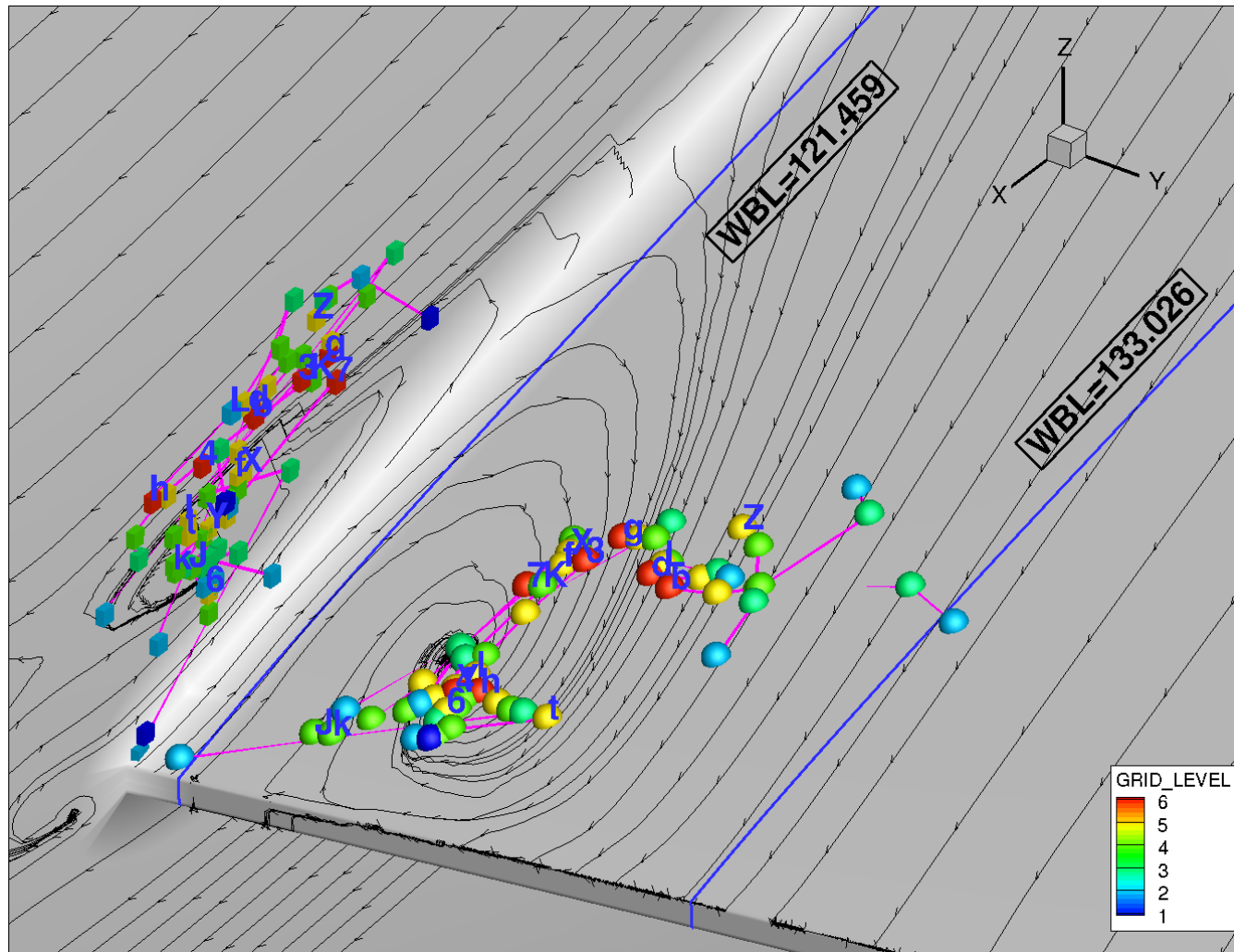
Side of Body Separation Bubble

1. Reported some level of SOB Separation:
I, J, K, L, X, Y, Z, 3, 4, 5, 6, 7, 9,
b, d, f, g, h, k, t, α , β , δ , γ , λ , π
2. Reported no SOB Separation (SOB File Provided):
U, V, W, 2, e, m, n, q, r
3. No Report (No SOB File Provided):
A, B, C, D, E, F, G, H, M, N, O, P, Q, R, S, T, 8, a

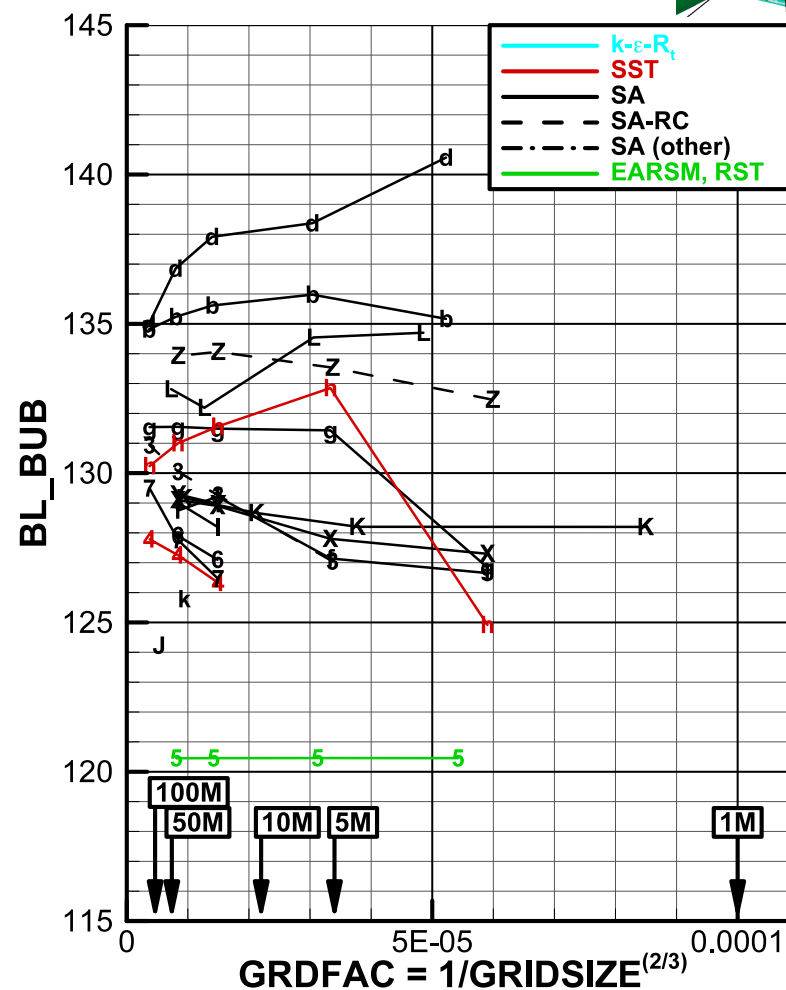
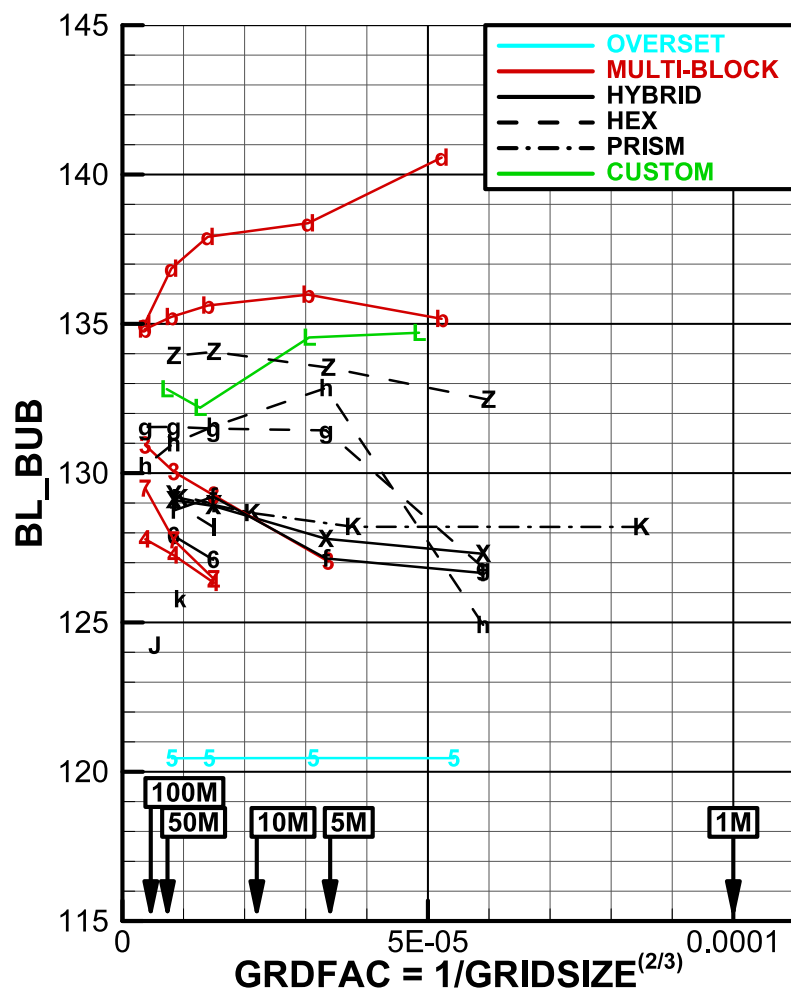
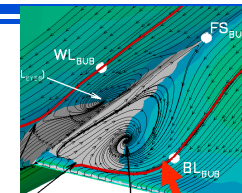
Example Grid Refinement: with Dataset “f” only



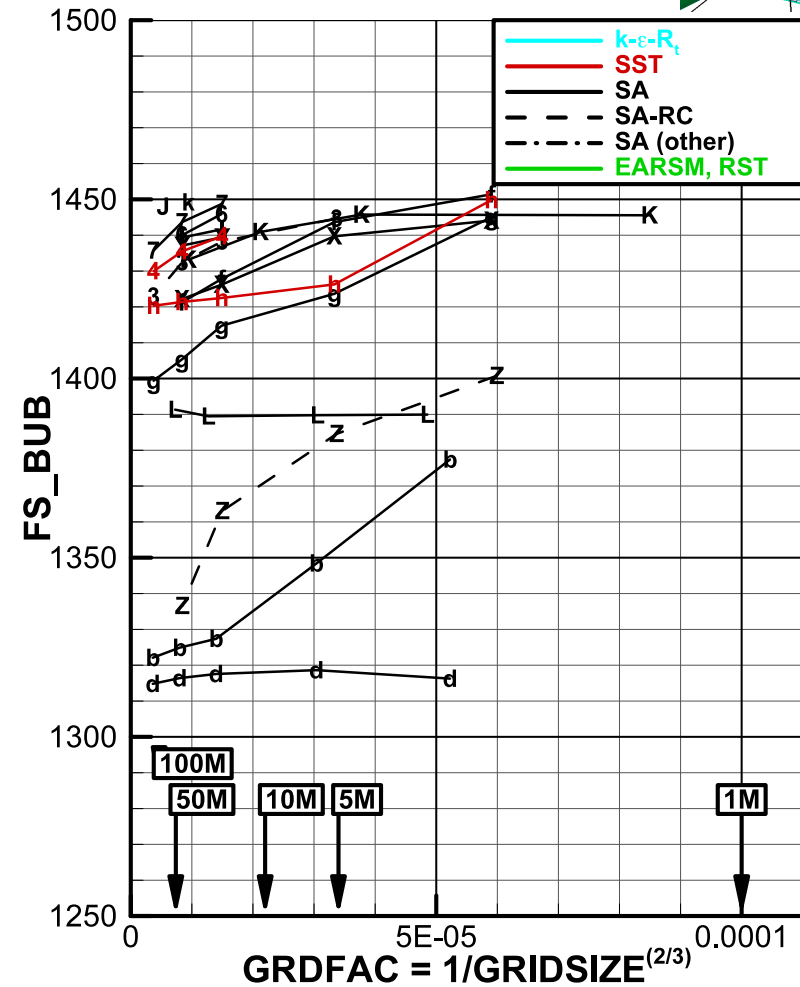
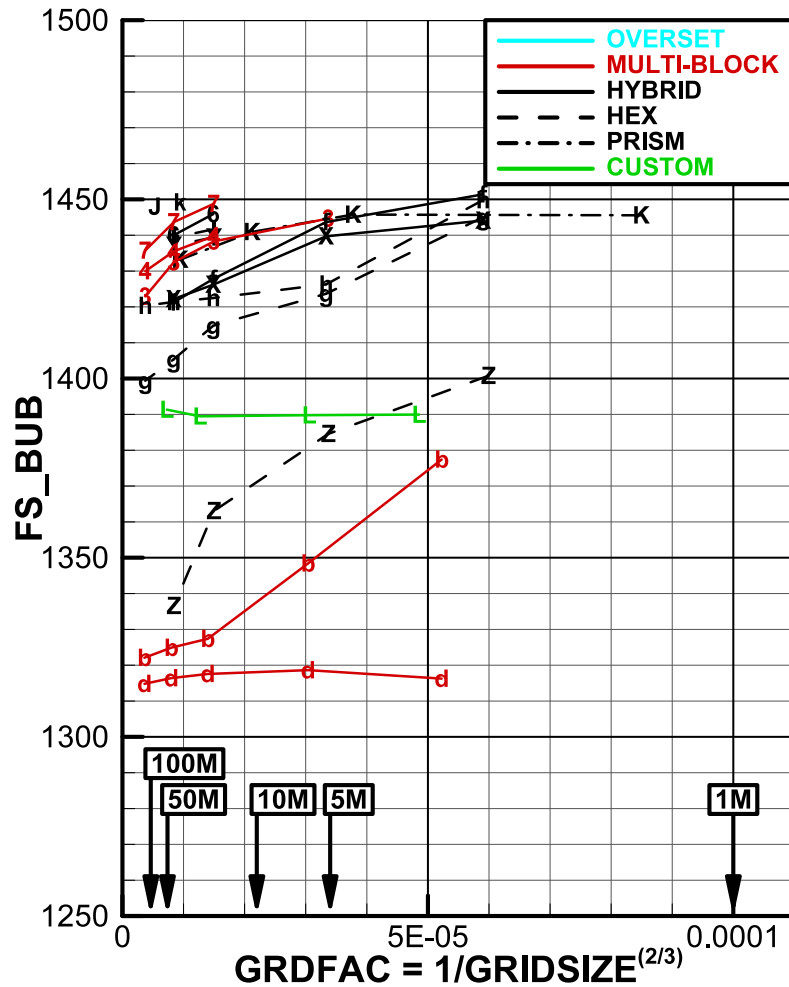
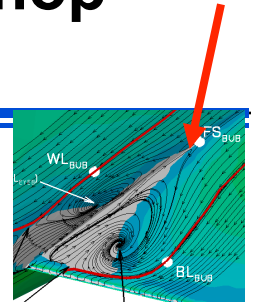
Grid Refinement: All Data



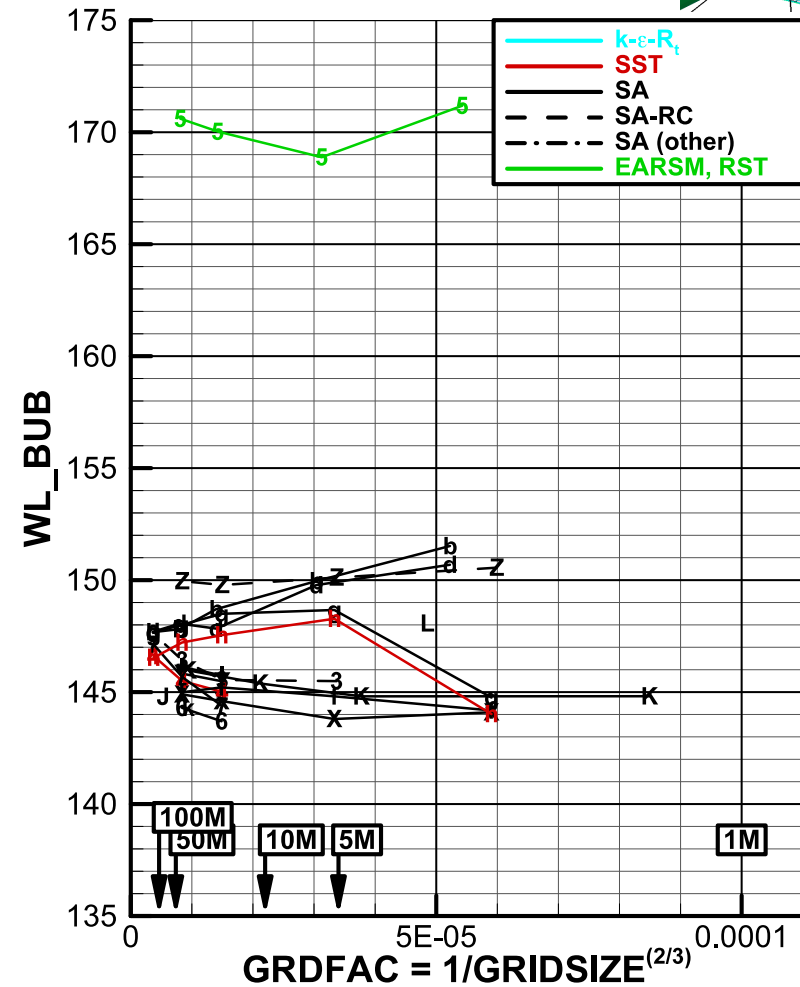
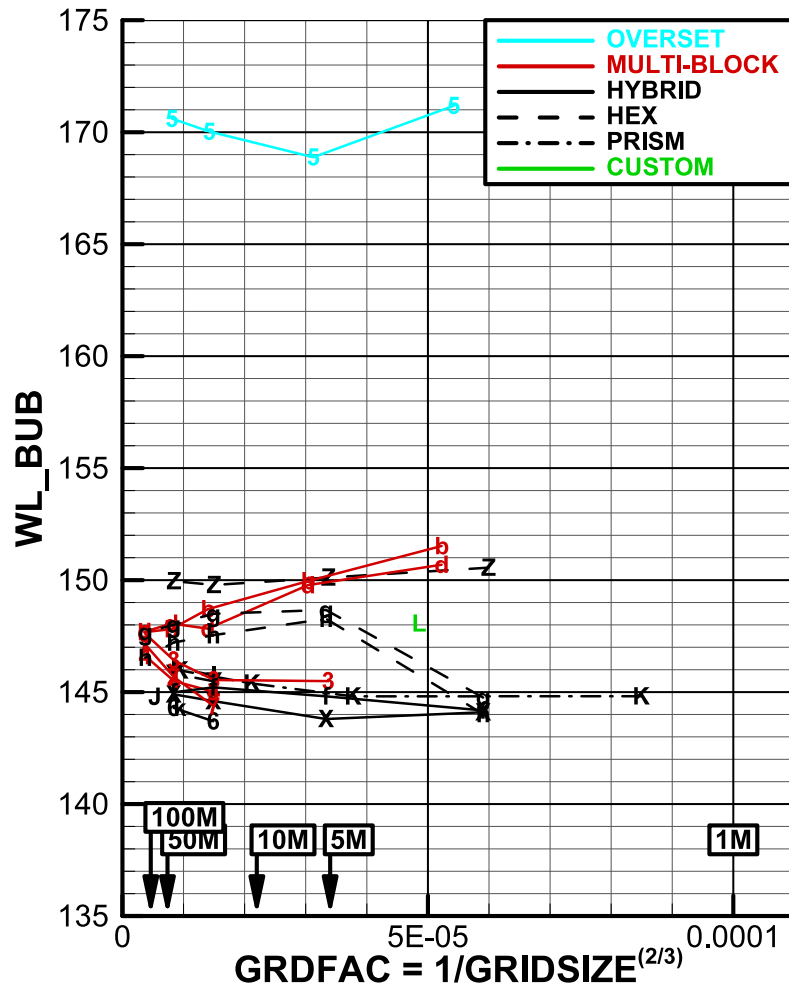
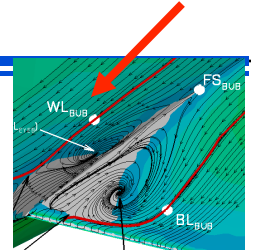
Bubble Width (Wing): Case 1 By Grid Type and Turbulence Model



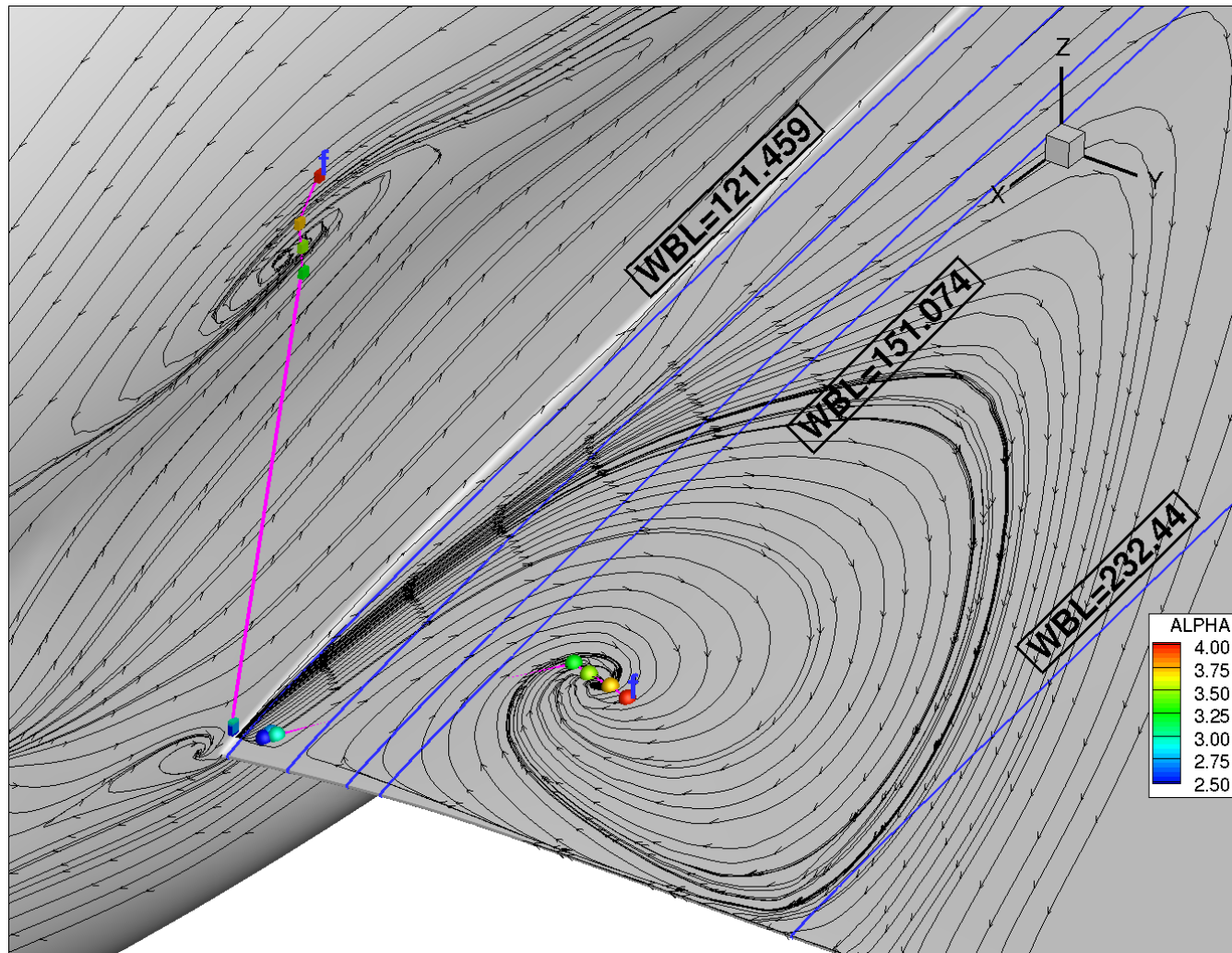
Bubble Leading Edge: Case 1 By Grid Type and Turbulence Model



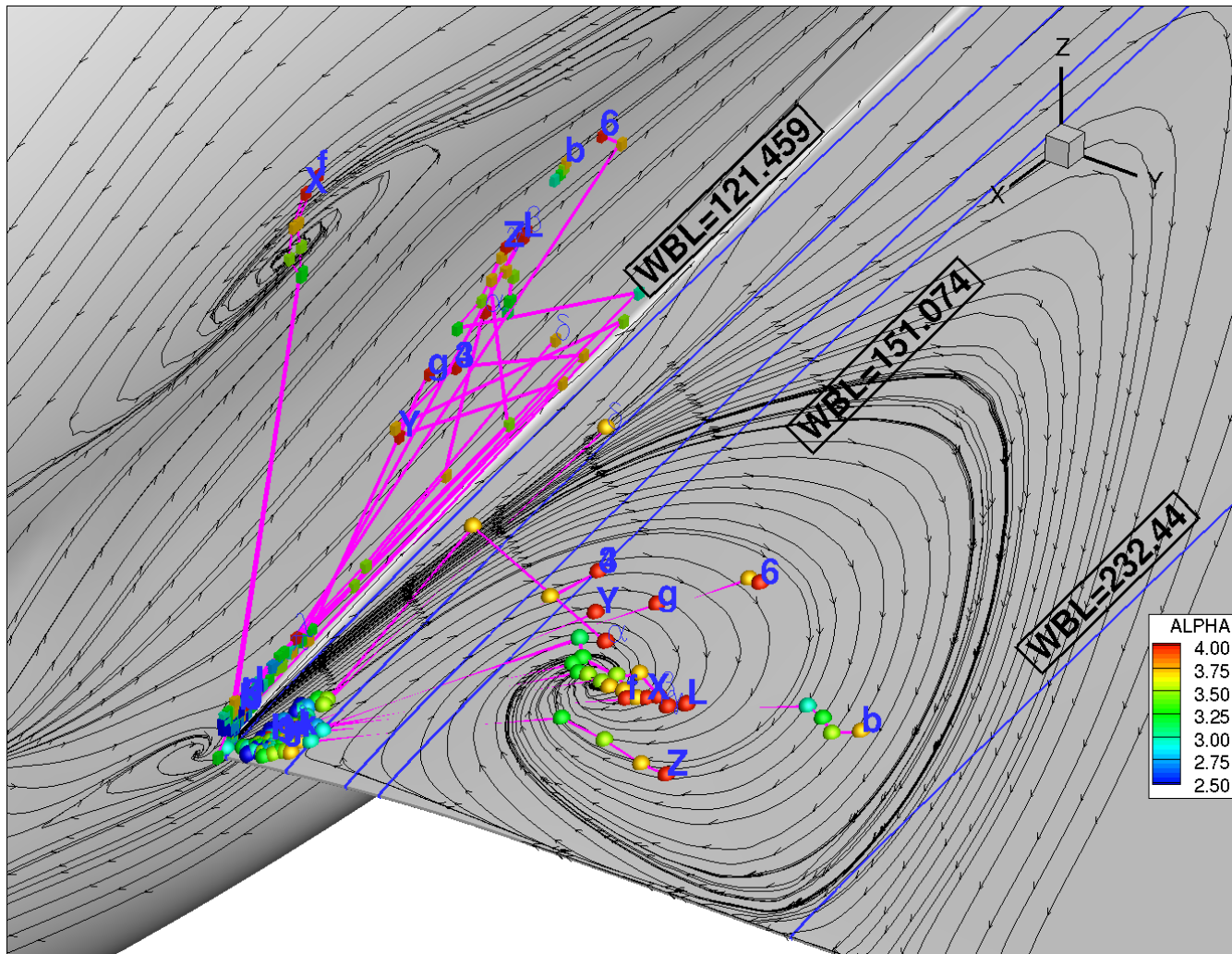
Bubble Height (Fuselage): Case 1 By Grid Type and Turbulence Model



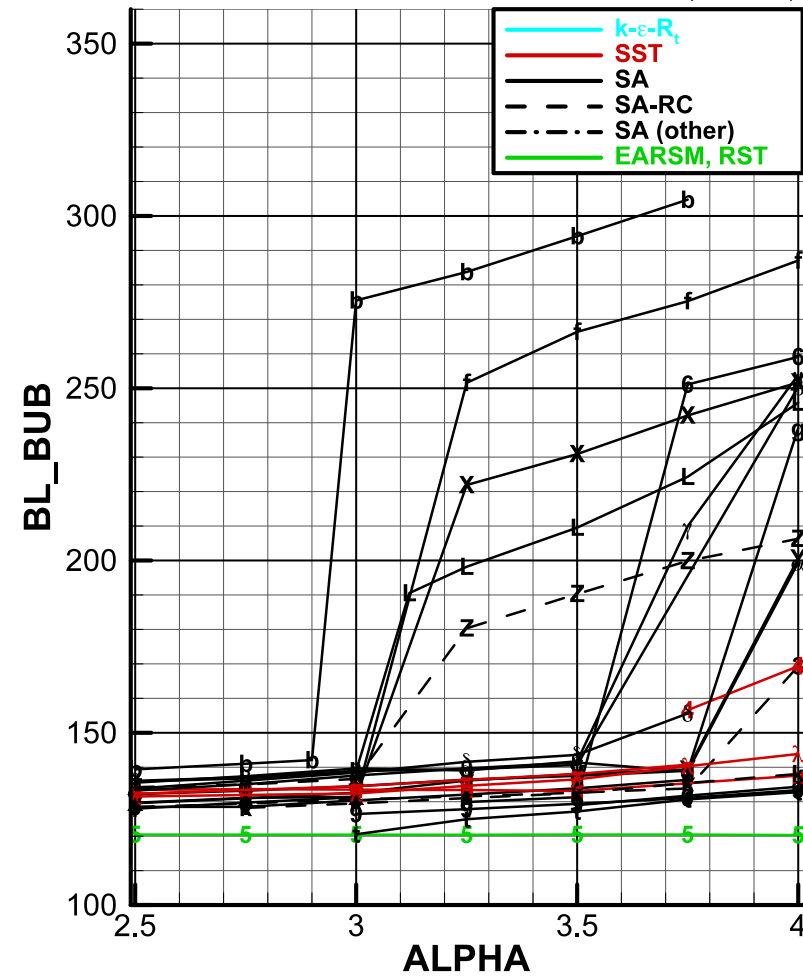
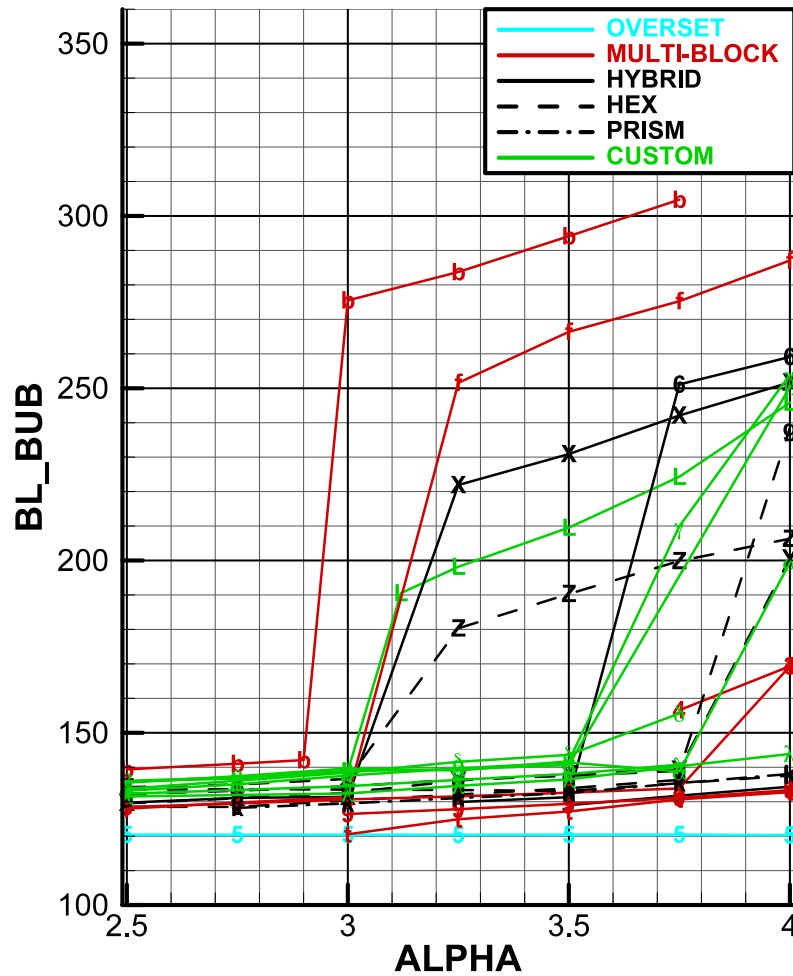
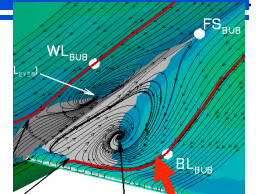
Example Alpha Sweep: with Dataset “f” only



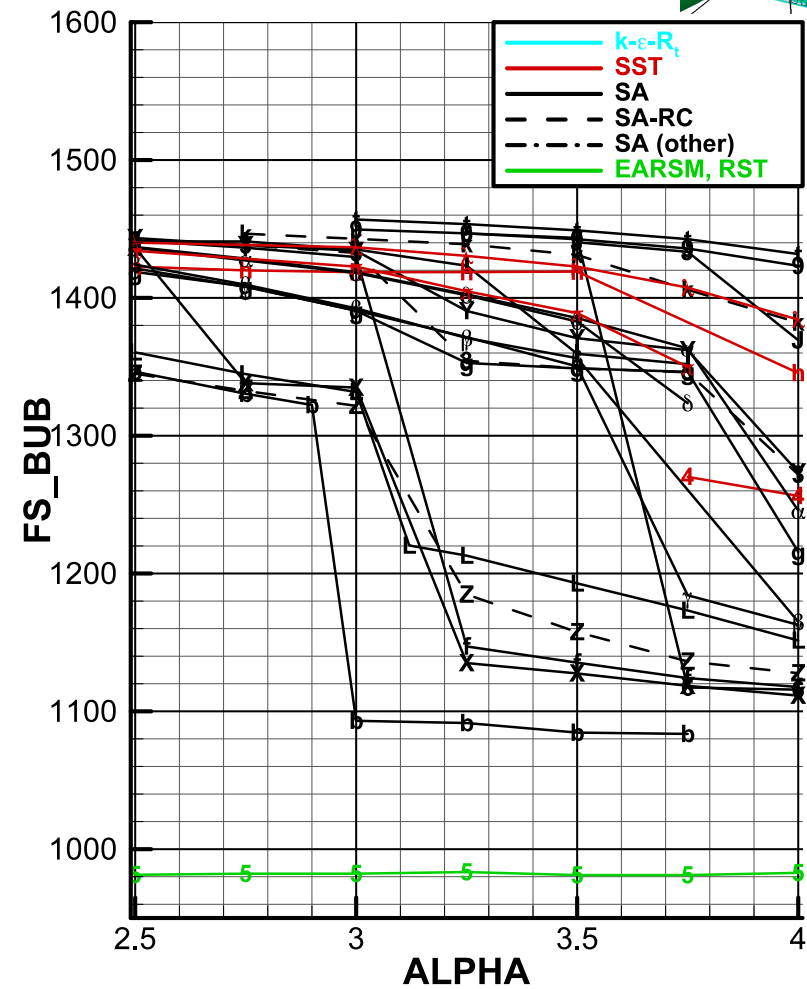
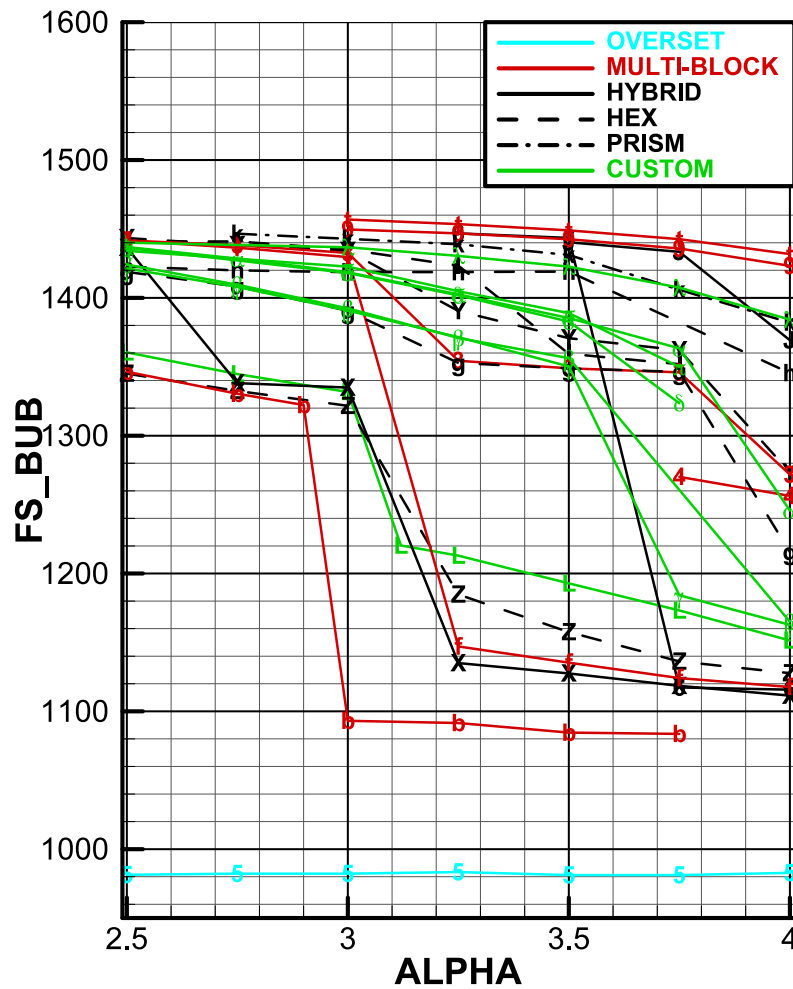
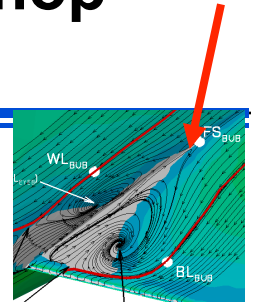
Alpha Sweep: All Data



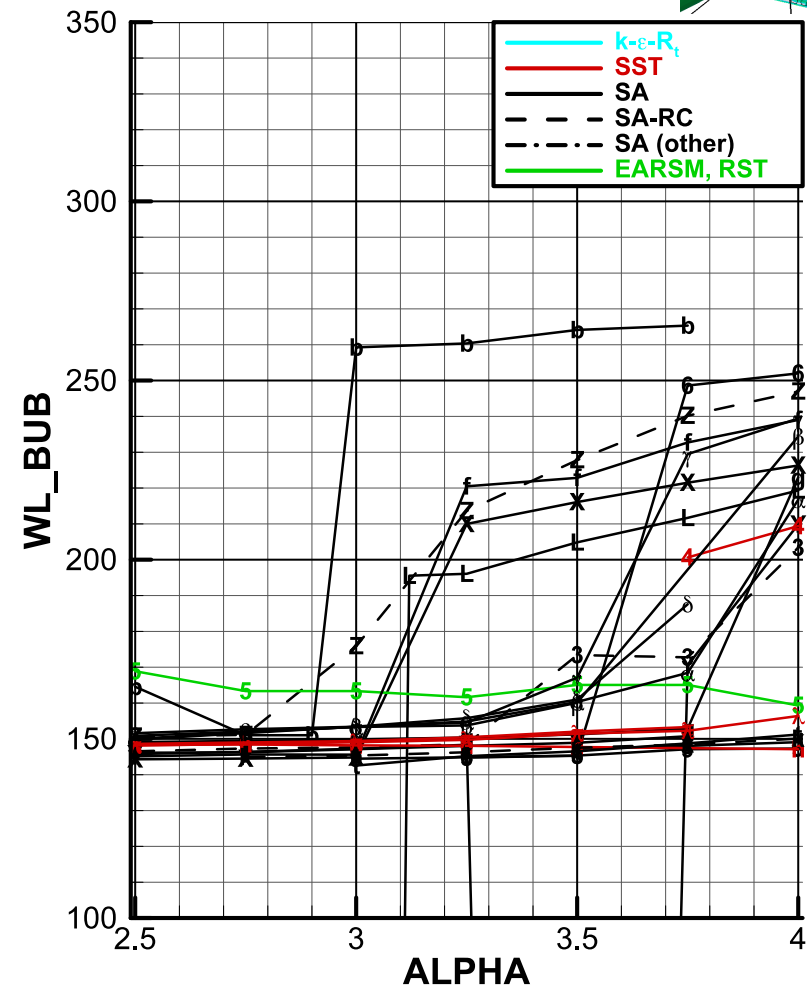
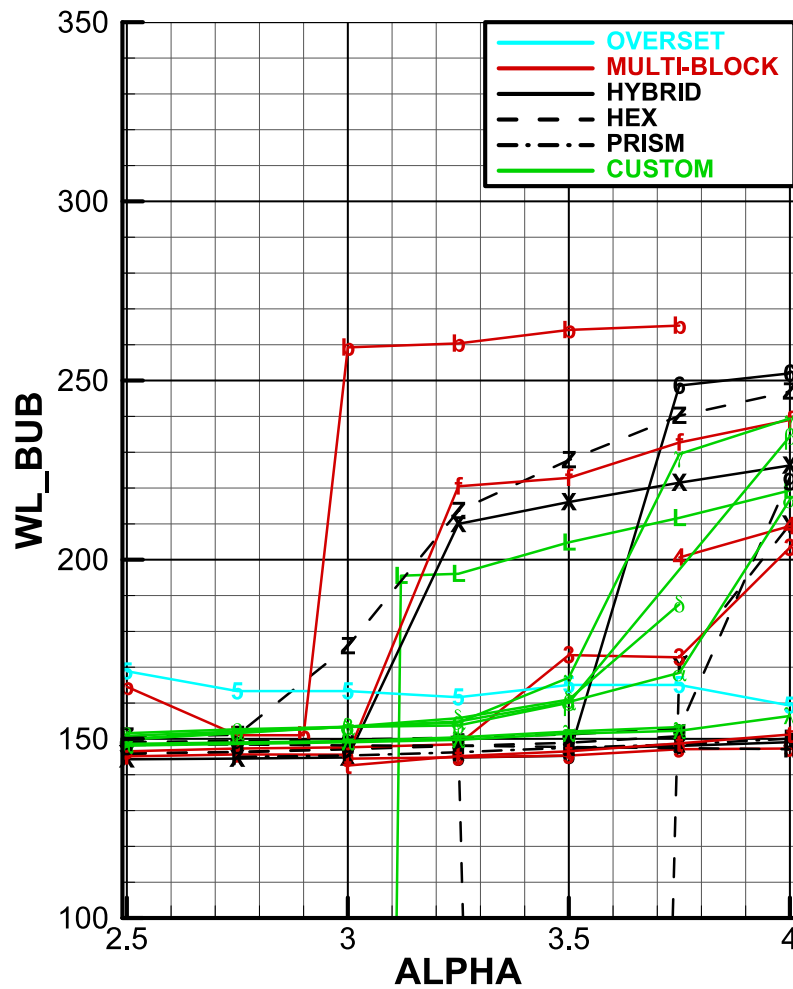
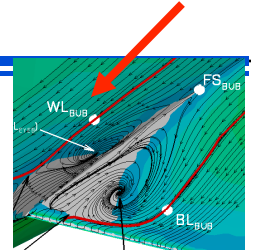
Bubble Width (Wing): Case 2 By Grid Type and Turbulence Model



Bubble Leading Edge: Case 2 By Grid Type and Turbulence Model



Bubble Height (Fuselage): Case 2 By Grid Type and Turbulence Model

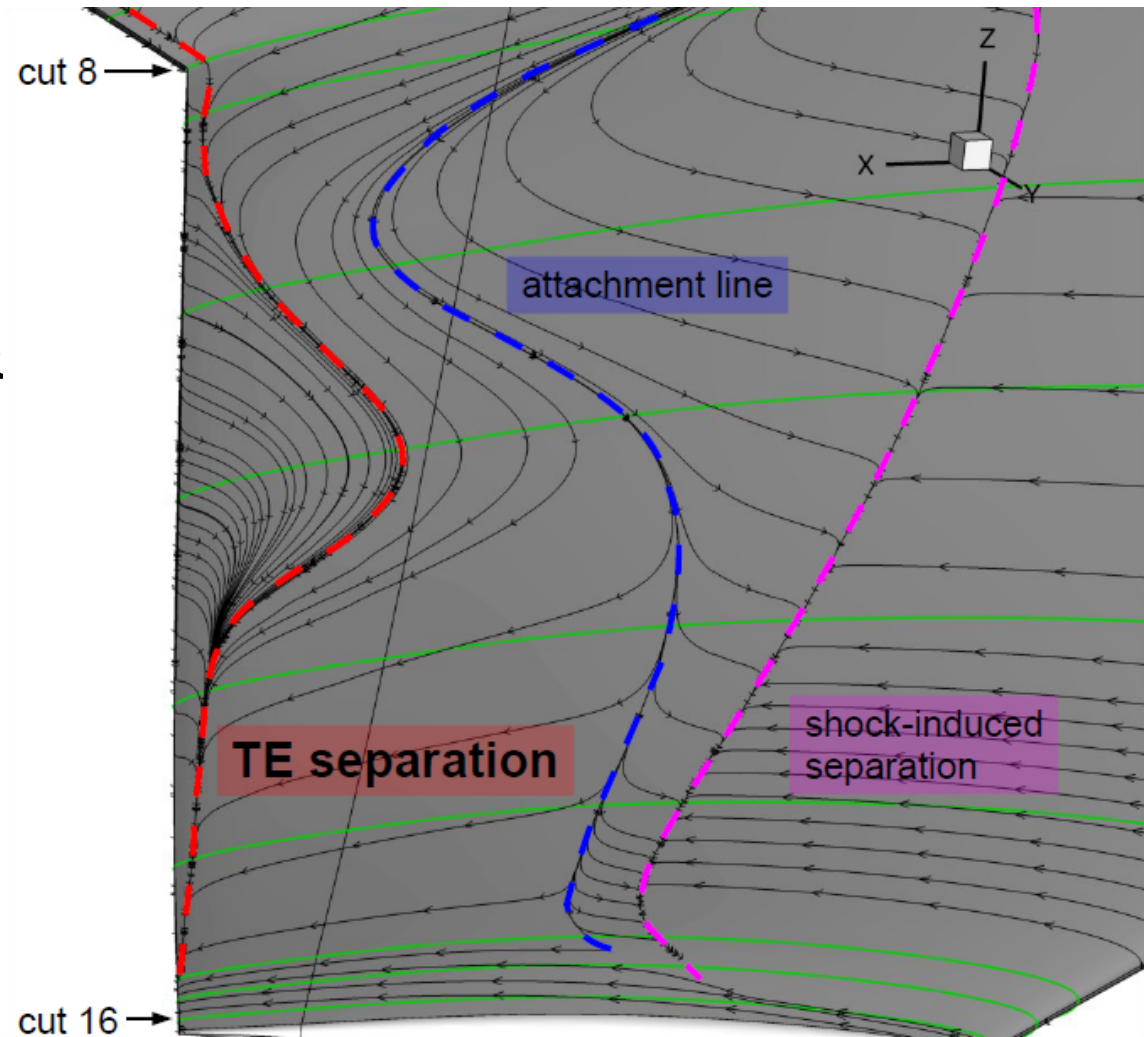


Conclusions from Separation Bubble:

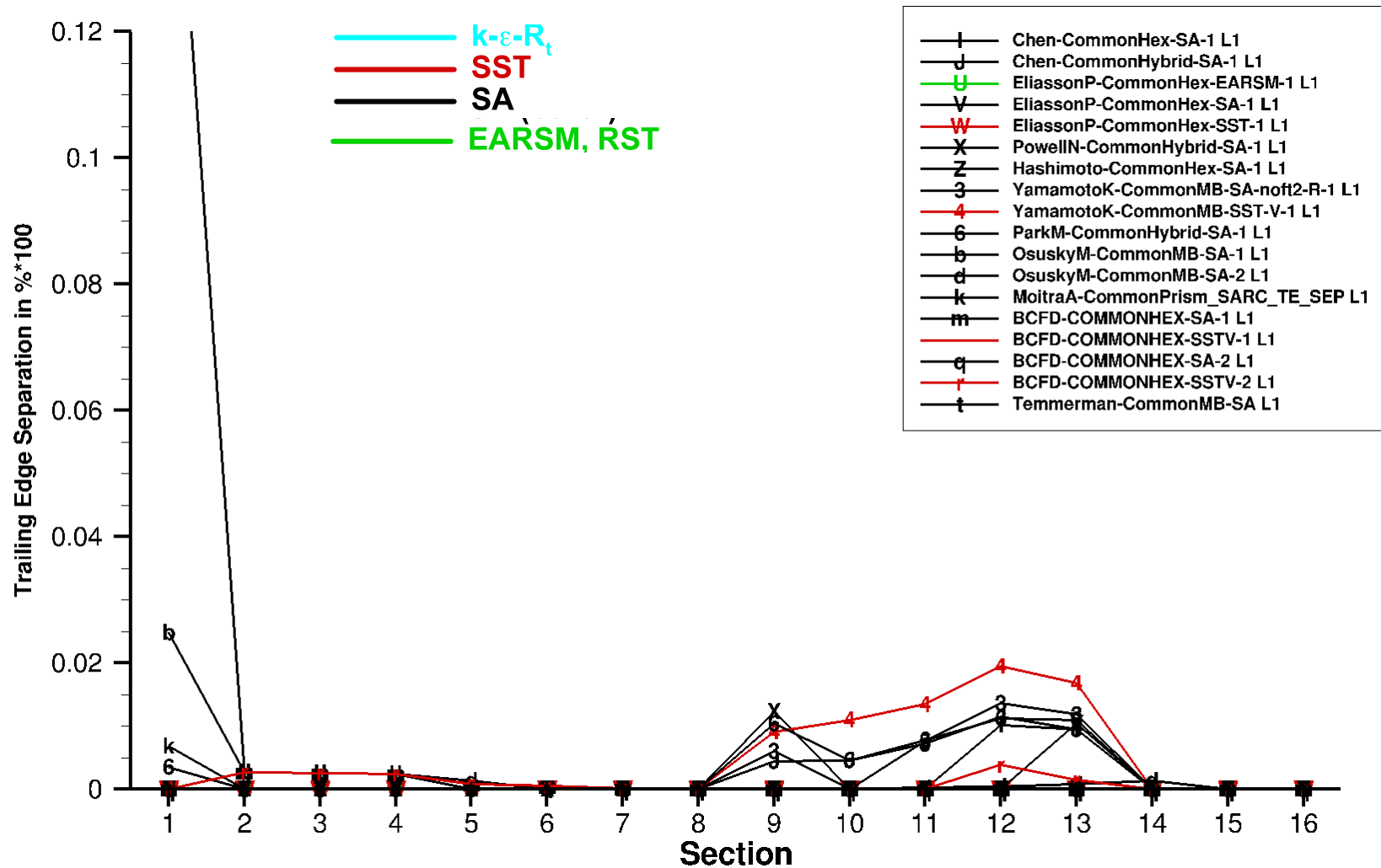
- Variation with grid level fairly consistent (note that coarse level grids do not have proper resolution)
- Some data sets show dramatic increase in bubble size at higher alpha
 - Mostly for Spalart-Allmaras results

Trailing Edge Separation:

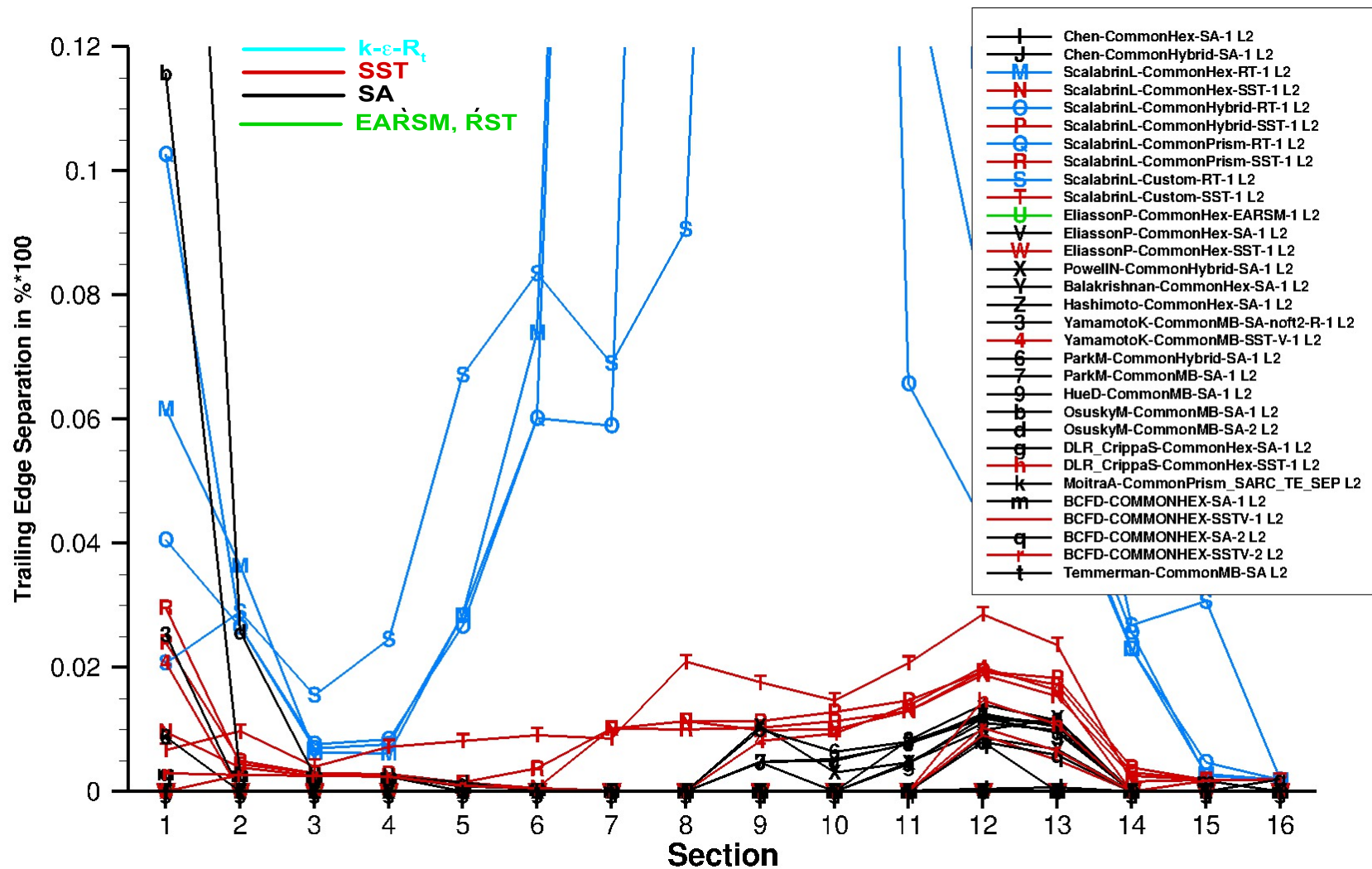
- DPW-4: C_f normal to TE < 0 as criteria
- For higher α more difficult to define & detect



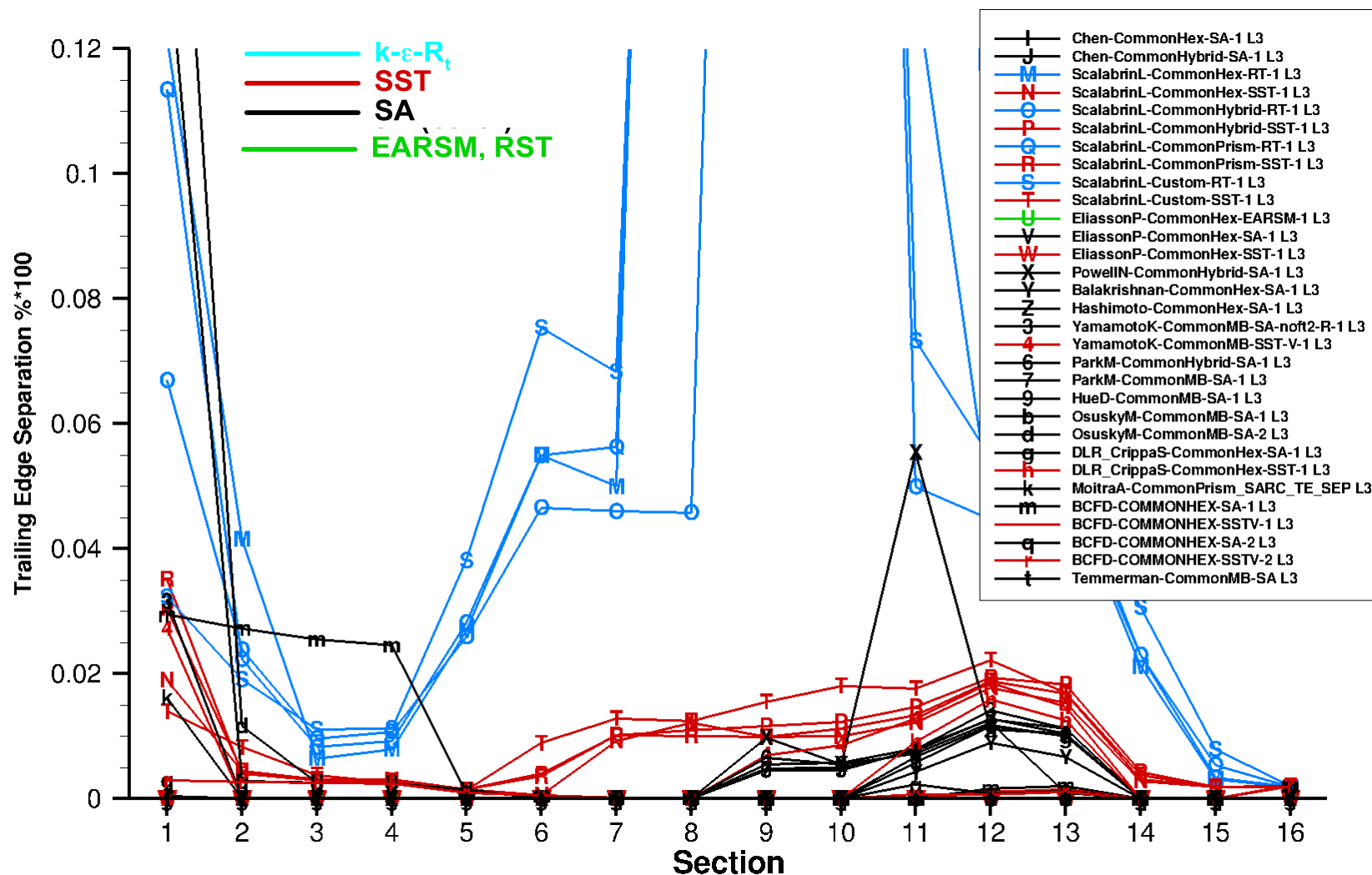
Case 1: Trailing Edge Separation, Level 1



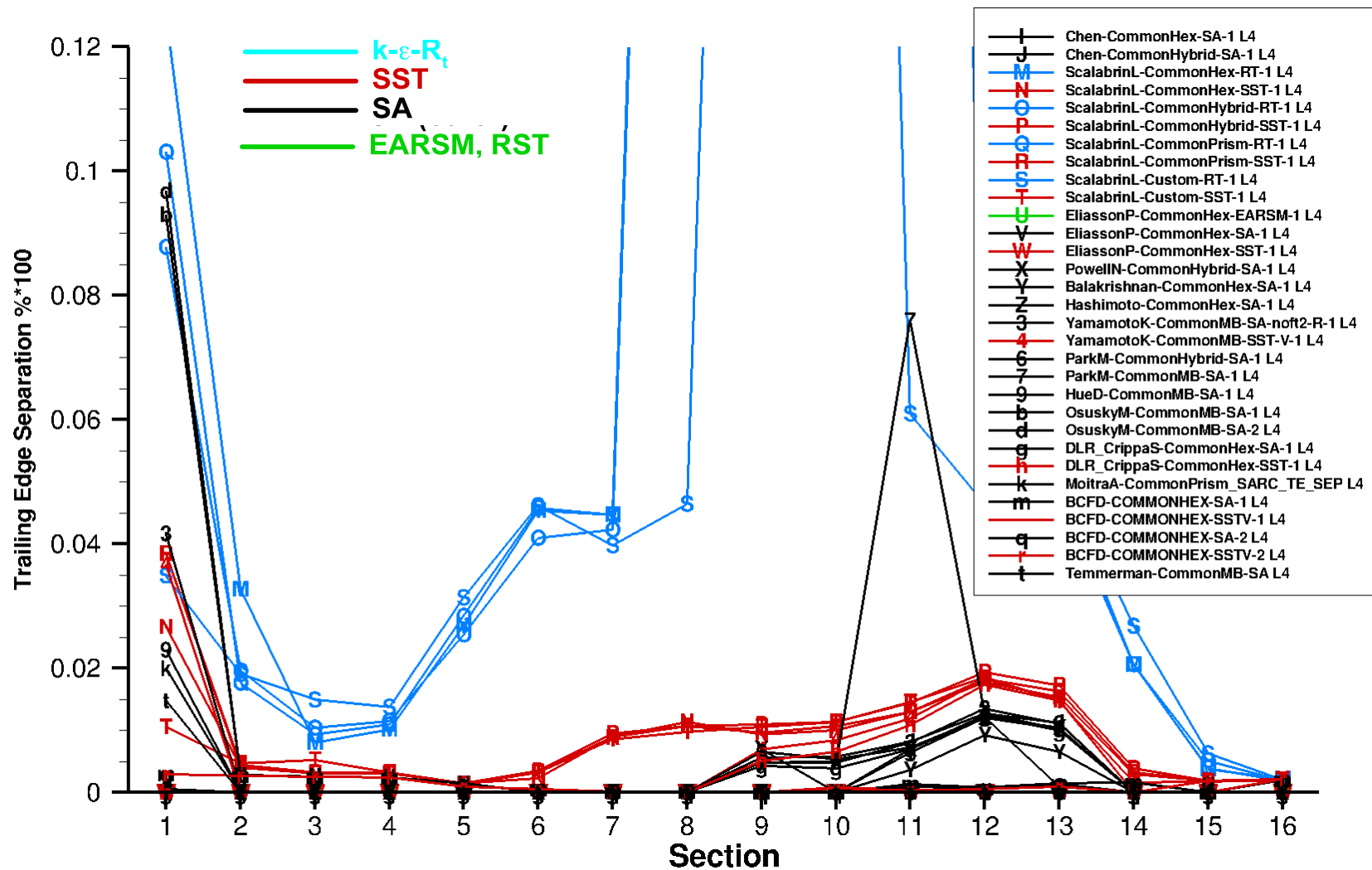
Case 1: Trailing Edge Separation, Level 2



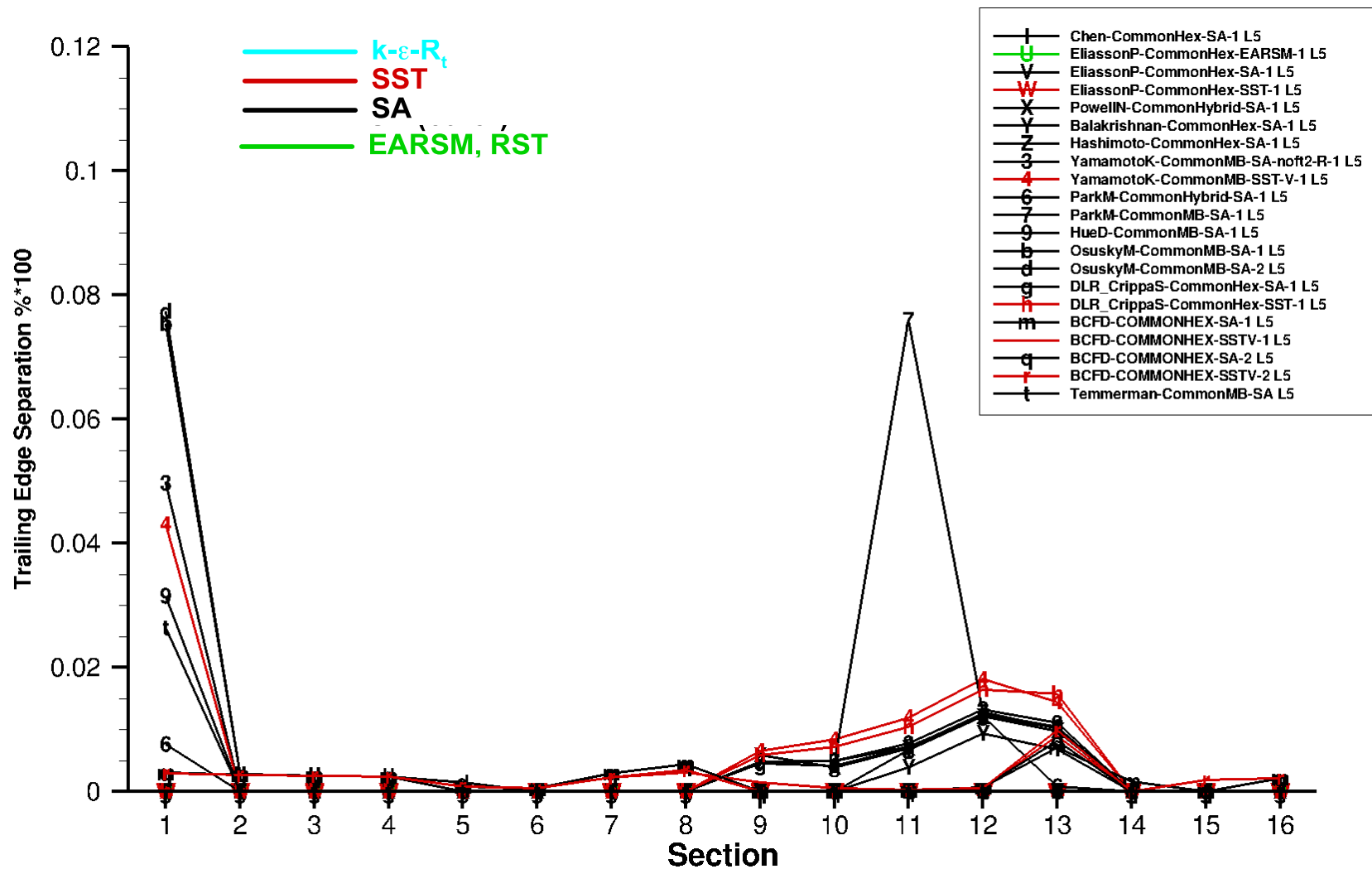
Case 1: Trailing Edge Separation, Level 3



Case 1: Trailing Edge Separation, Level 4



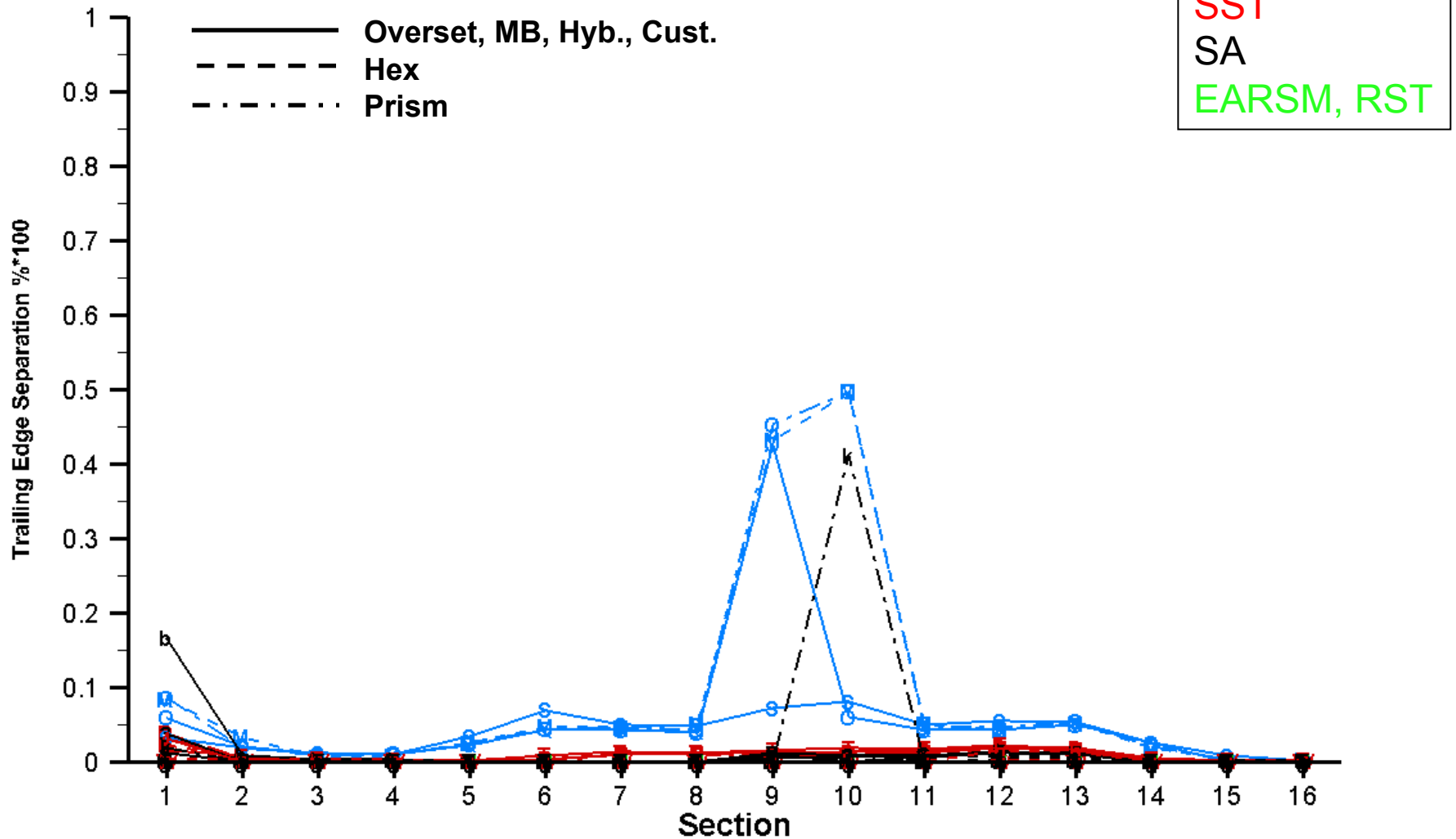
Case 1: Trailing Edge Separation, Level 5



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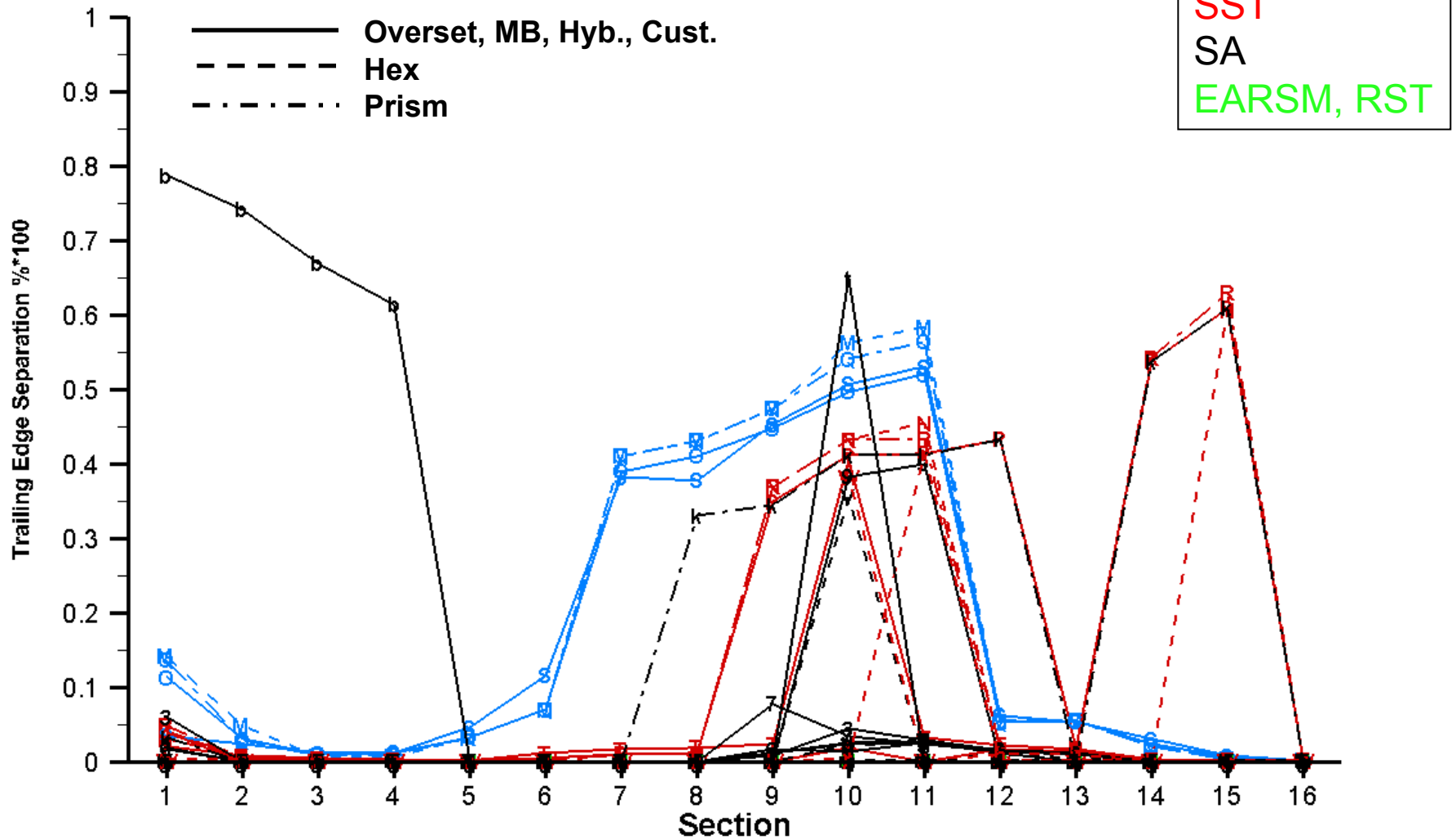
Trailing Edge Separation, Alpha = 2.5°



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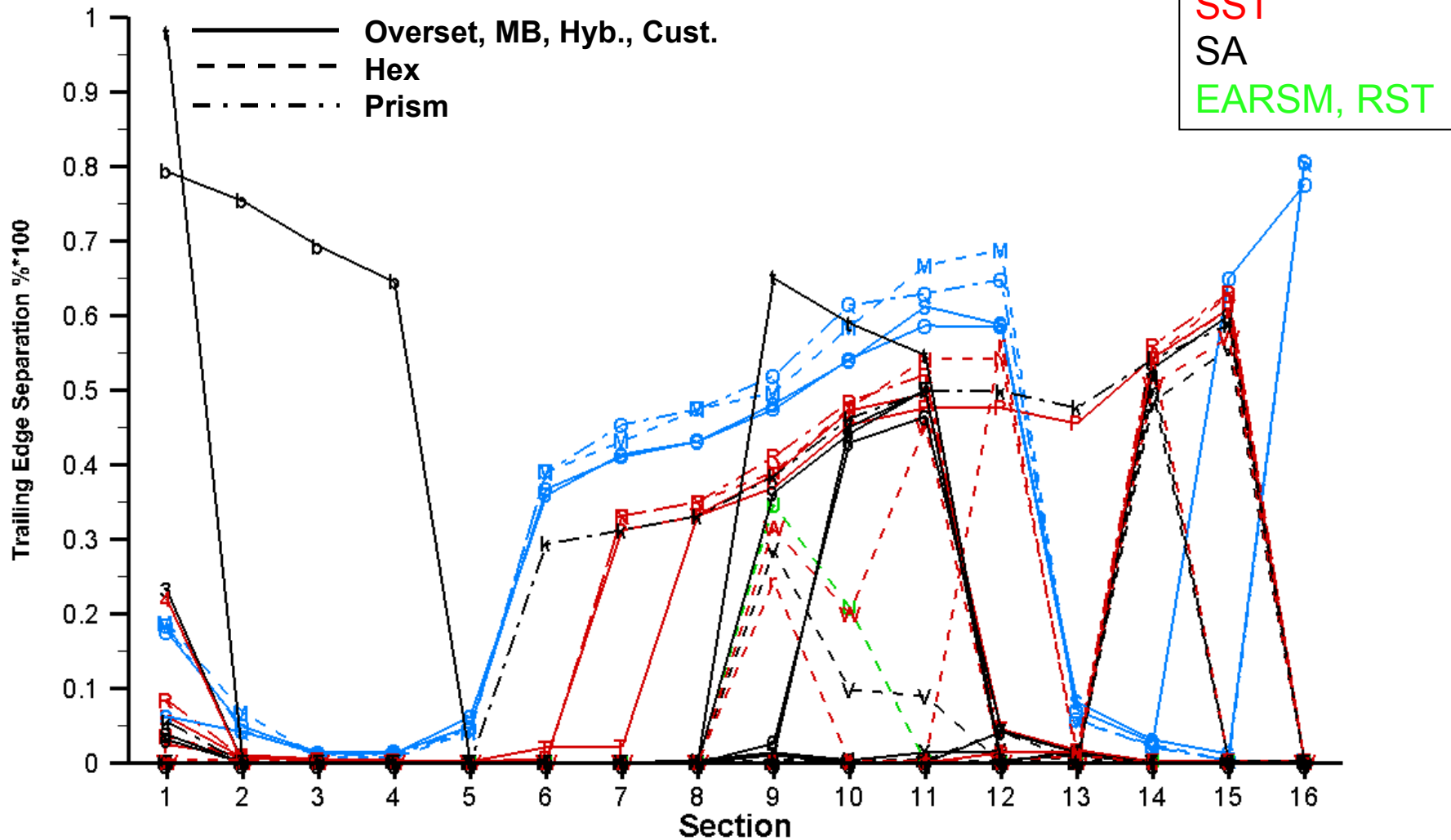
Trailing Edge Separation, Alpha = 3.0°



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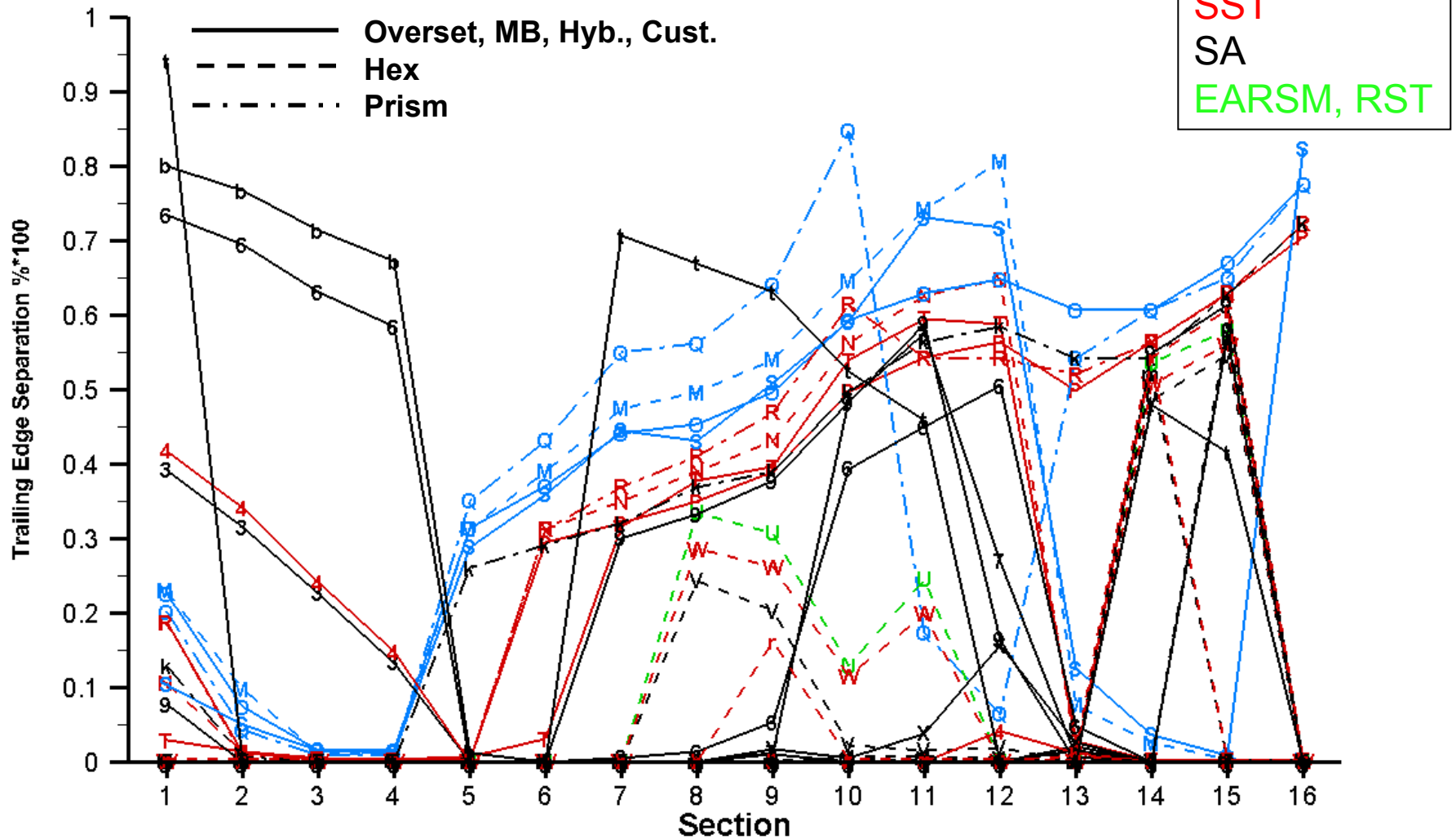
Trailing Edge Separation, Alpha = 3.5°



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Trailing Edge Separation, Alpha = 4.0°



Conclusions from Trailing Edge Separation:

- Case 1:
 - SA, SST show similar small TE sep $\leq 2\%$ between sections 8, ..., 14
 - Slightly larger for SST on coarse, medium grids
- Case 2:
 - Trend to extend towards sections 5 & 16 for $\alpha \geq 2.5^\circ$
 - No clear conclusion
- Overall check necessary whether same TE sep identification procedure has been applied

General Conclusions:

- Very successful workshop. **Thank You!**
 - 54 data submittals, many with parametric variations in grid type and/or turbulence model
- Still more variation than desired
 - Some improvement from DPW4: We are getting better
 - Mixed results from common grid study. Discretization and turbulence modeling are still a factor
- Drag comparisons to wind tunnel generally favorable
 - Variations similar between WT and CFD
 - ALPHA and CM_TOT offsets
 - Aeroelasticity

General Conclusions (Cont'd):

- Force/Moment predictions better at $\alpha=2.5^\circ$
 - Less separation
 - Bigger spread at $\alpha=4.0^\circ$
- Pressures consistent with Force/Moments
 - Correlation outboard supports aeroelastic effects
 - Wide variation in α for shock separation
- Large variations in separation prediction
 - SOB Separation
 - TE Separation and Buffet onset α
 - Is RANS good enough? Is flow steady?

Further Study:

- Check SOB/TE separation with wind tunnel data
 - Is flow visualization data available?
- Include static aeroelastics in CFD
 - Needed to match wind tunnel data
- Include boundary layer transition model
 - Forced/Free
- Unsteady RANS?
 - Will only help if flow is unsteady
- LES/DES?
 - DES only helps for off-body separation
 - LES (beyond current SOA?)



Applied Aerodynamics
Technical Committee

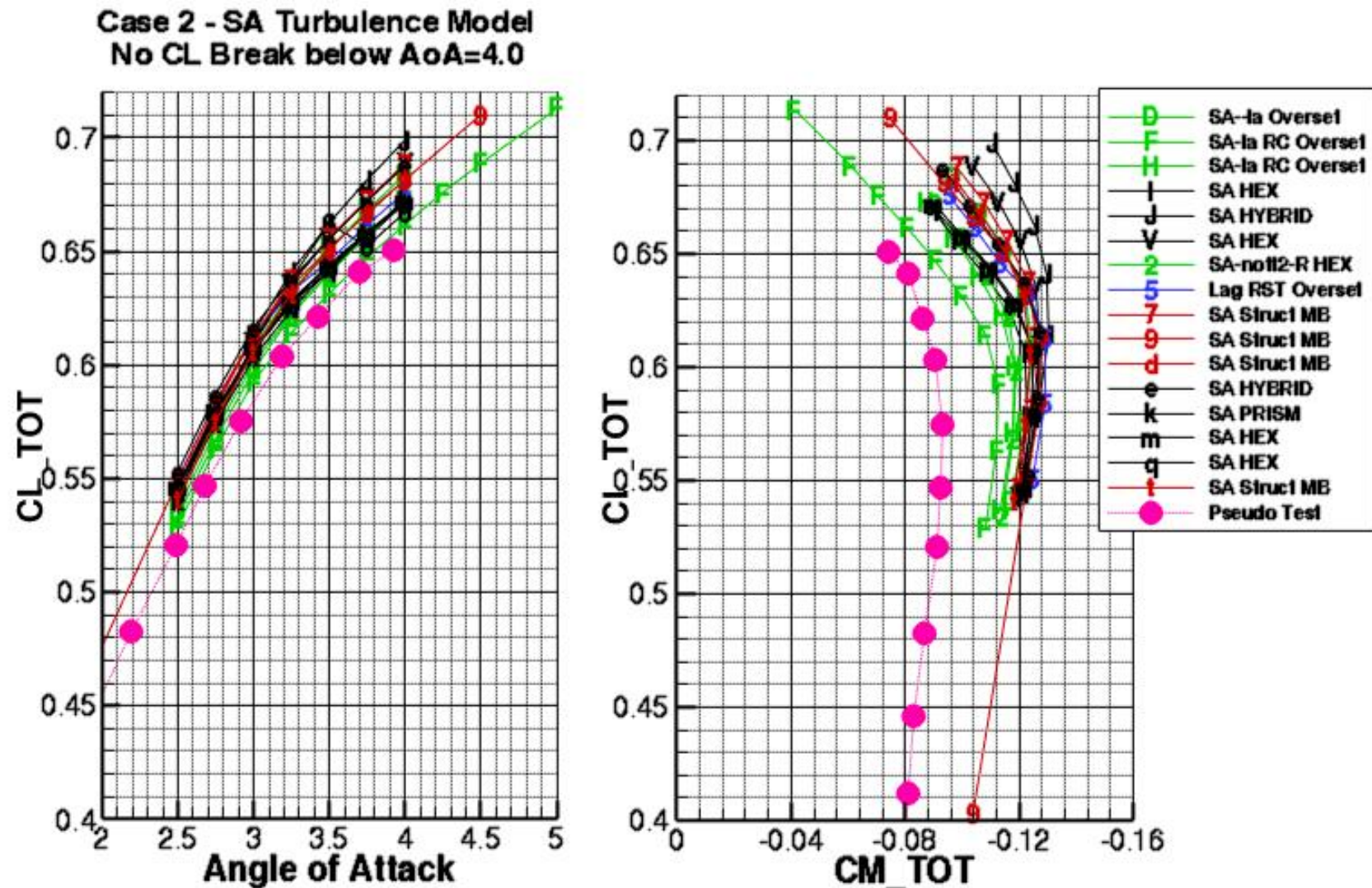
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Backup

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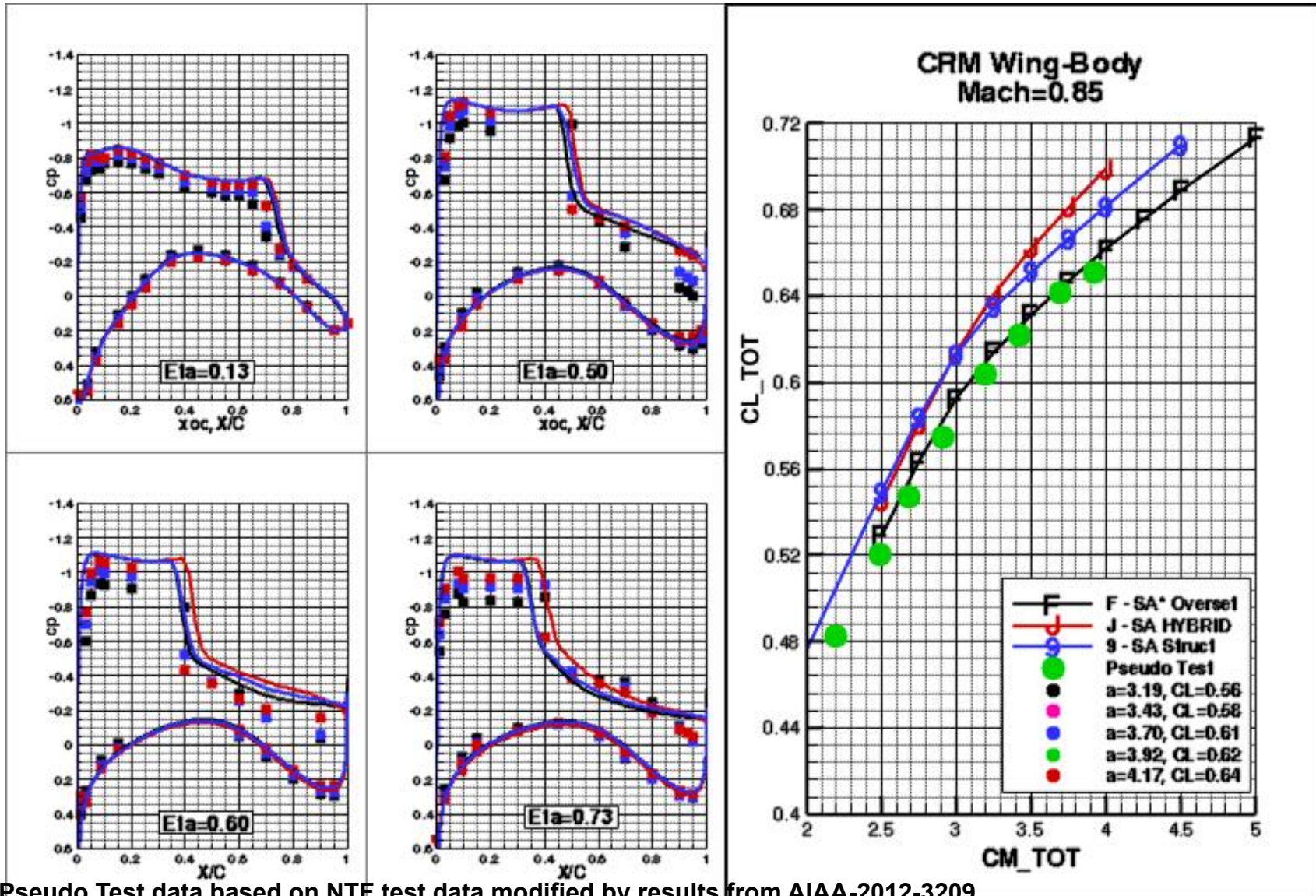
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Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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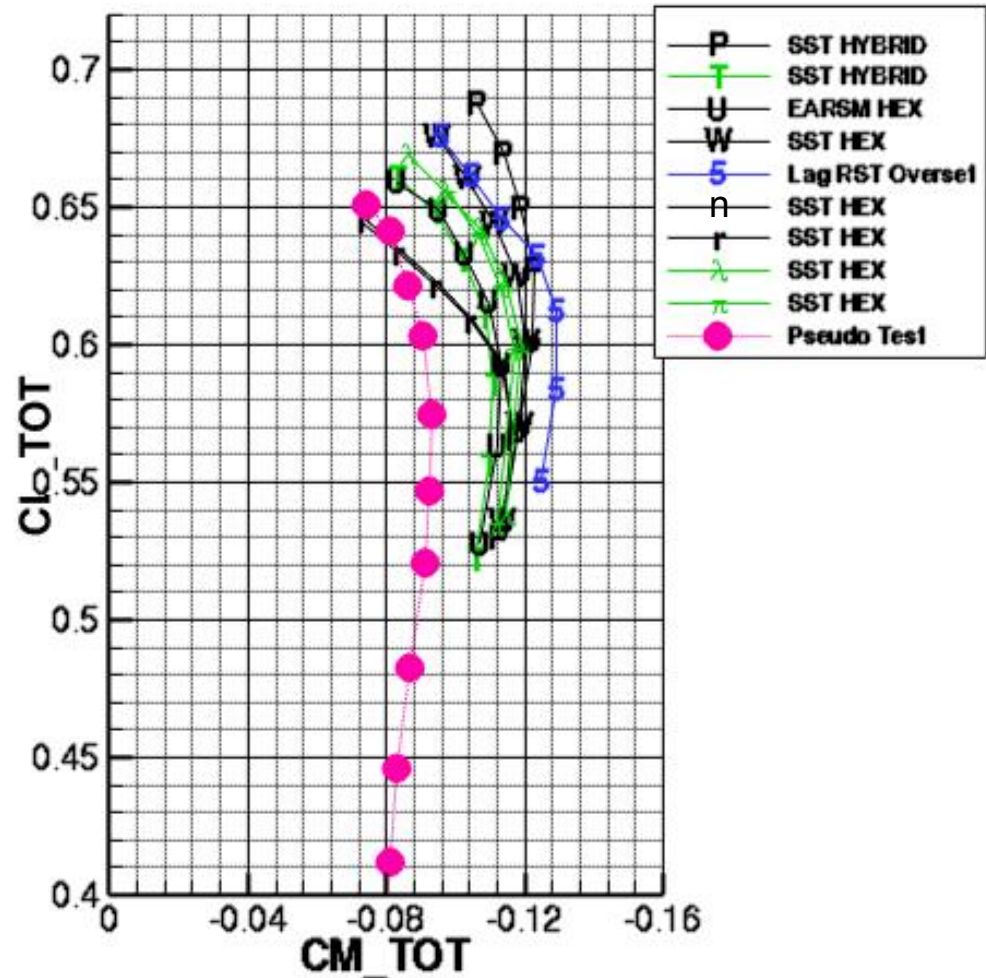
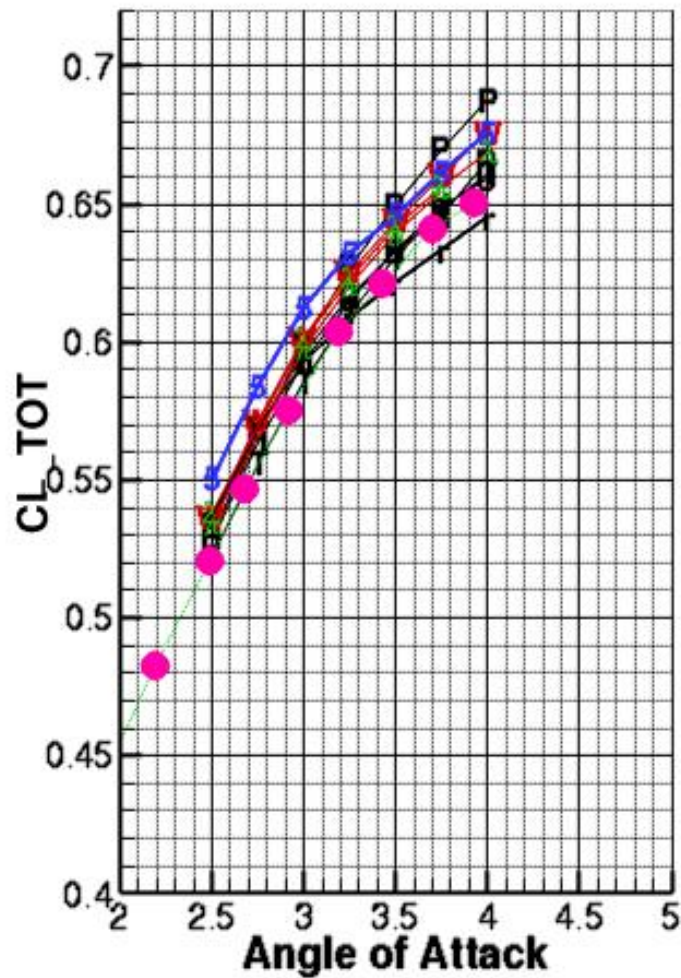


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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Case 2 - SST and Other
No CL Break below $\text{AoA}=4.0$



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